

Overview of NDCX-II Physics Design and Comments on final beam-lines for a driver^{*}

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Workshop on Accelerators for Heavy Ion Inertial Fusion
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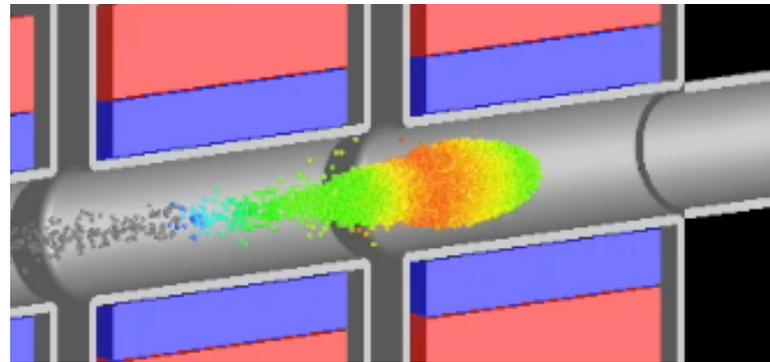


The Heavy Ion Fusion Science
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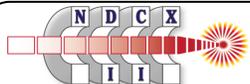


^{*} This work was performed under the auspices of the U.S. Department of Energy by Lawrence Livermore National Security, LLC, Lawrence Livermore National Laboratory under Contract DE-AC52-07NA27344, by LBNL under Contract DE-AC02-05CH11231, and by PPPL under Contract DE-AC02-76CH03073.

Overview of NDCX-II Physics Design

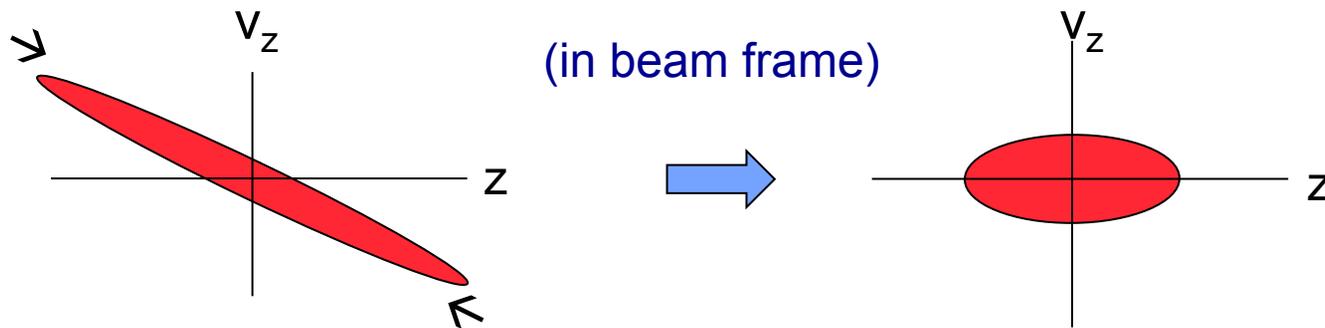


Beam traversing an acceleration gap

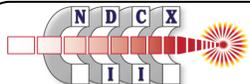
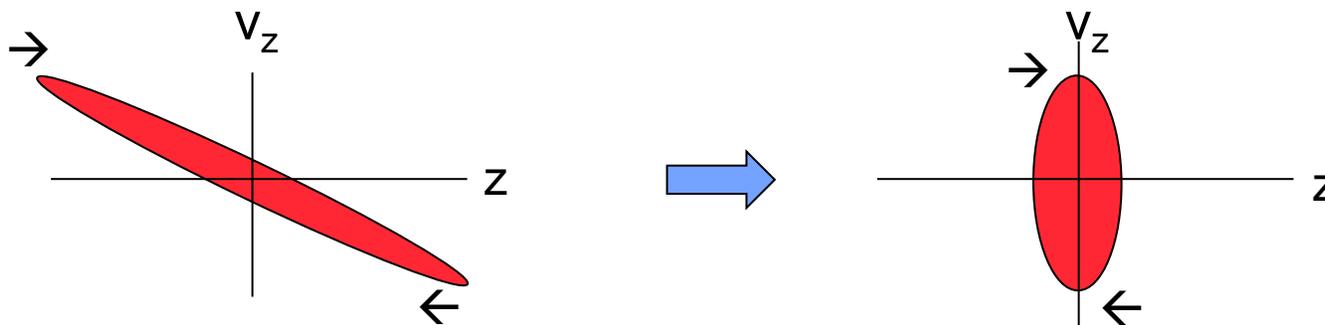


The drift compression process is used to shorten an ion bunch

- Induction cells impart a head-to-tail velocity gradient (“tilt”) to the beam
 - The beam shortens as it “drifts” down the beam line
-
- In **non-neutral drift compression**, the space charge force opposes (“stagnates”) the inward flow, leading to a nearly mono-energetic compressed pulse:



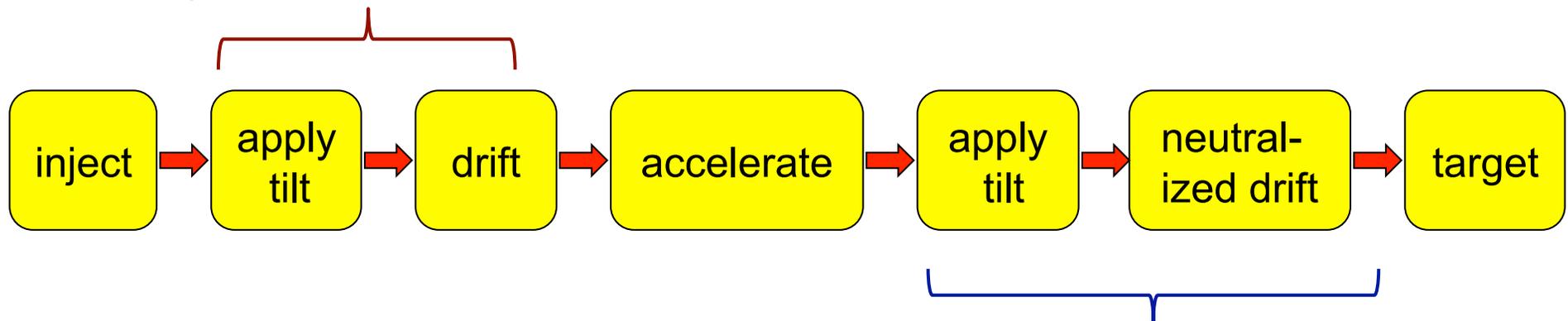
-
- In **neutralized drift compression**, the space charge force is eliminated, resulting in a shorter pulse but a larger velocity spread:



Drift compression is used twice in NDCX-II

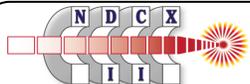
Initial non-neutral pre-bunching for:

- better use of induction-core Volt-seconds
- early use of 70-ns 250-kV Blumlein power supplies from ATA

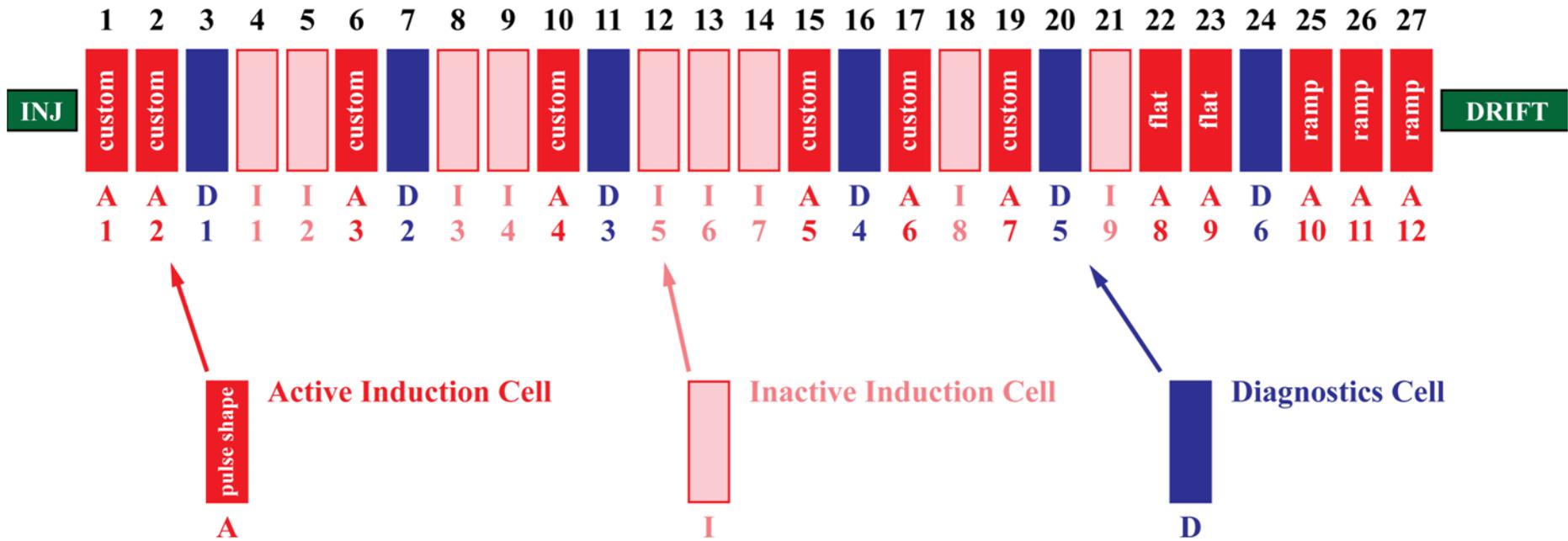


Final neutralized drift compression onto the target

- Electrons in plasma move so as to cancel the beam's electric field
- Require $n_{\text{plasma}} > n_{\text{beam}}$ for this to work well

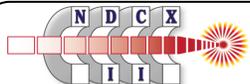
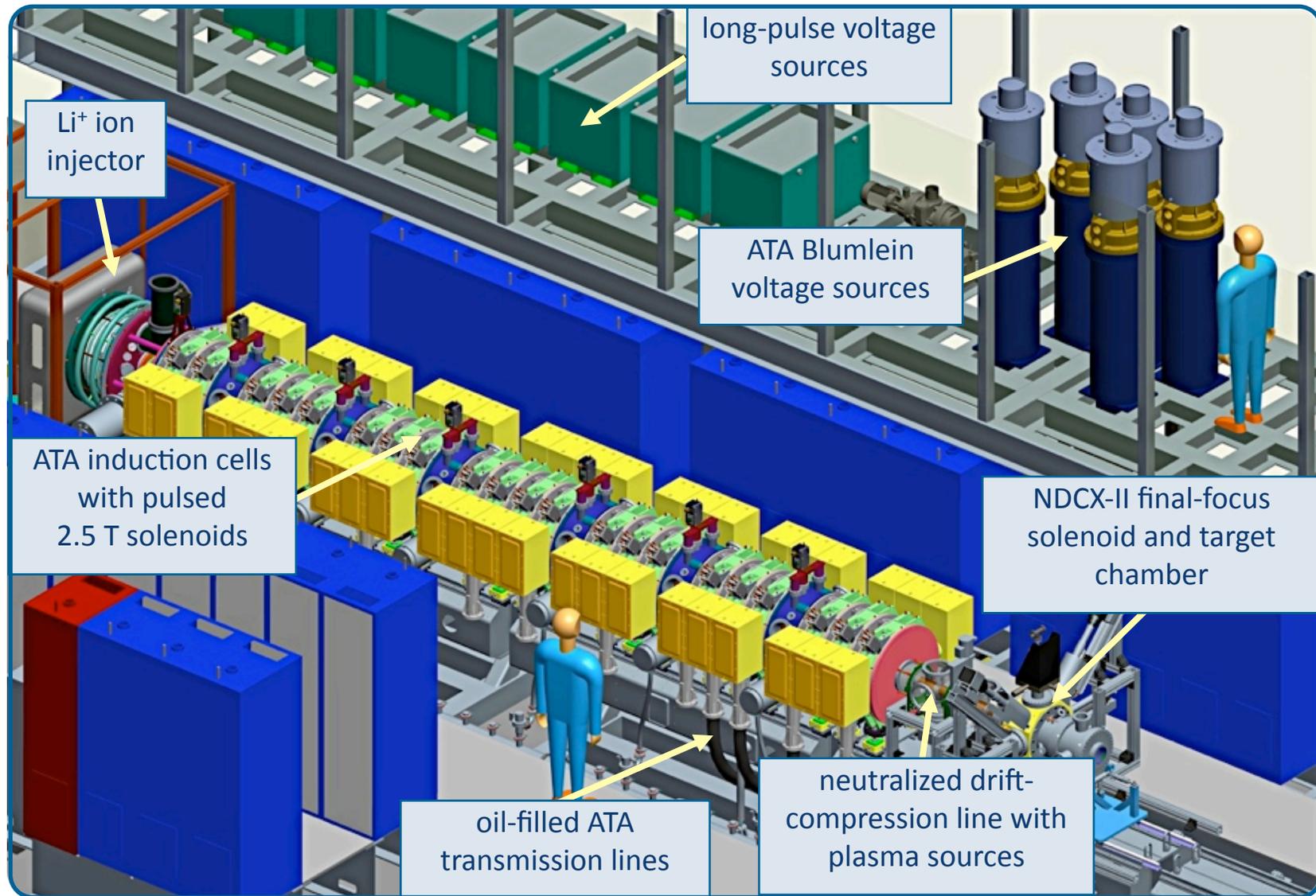


The baseline hardware configuration is as presented during the April 2010 DOE Project Review

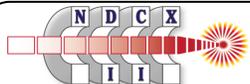
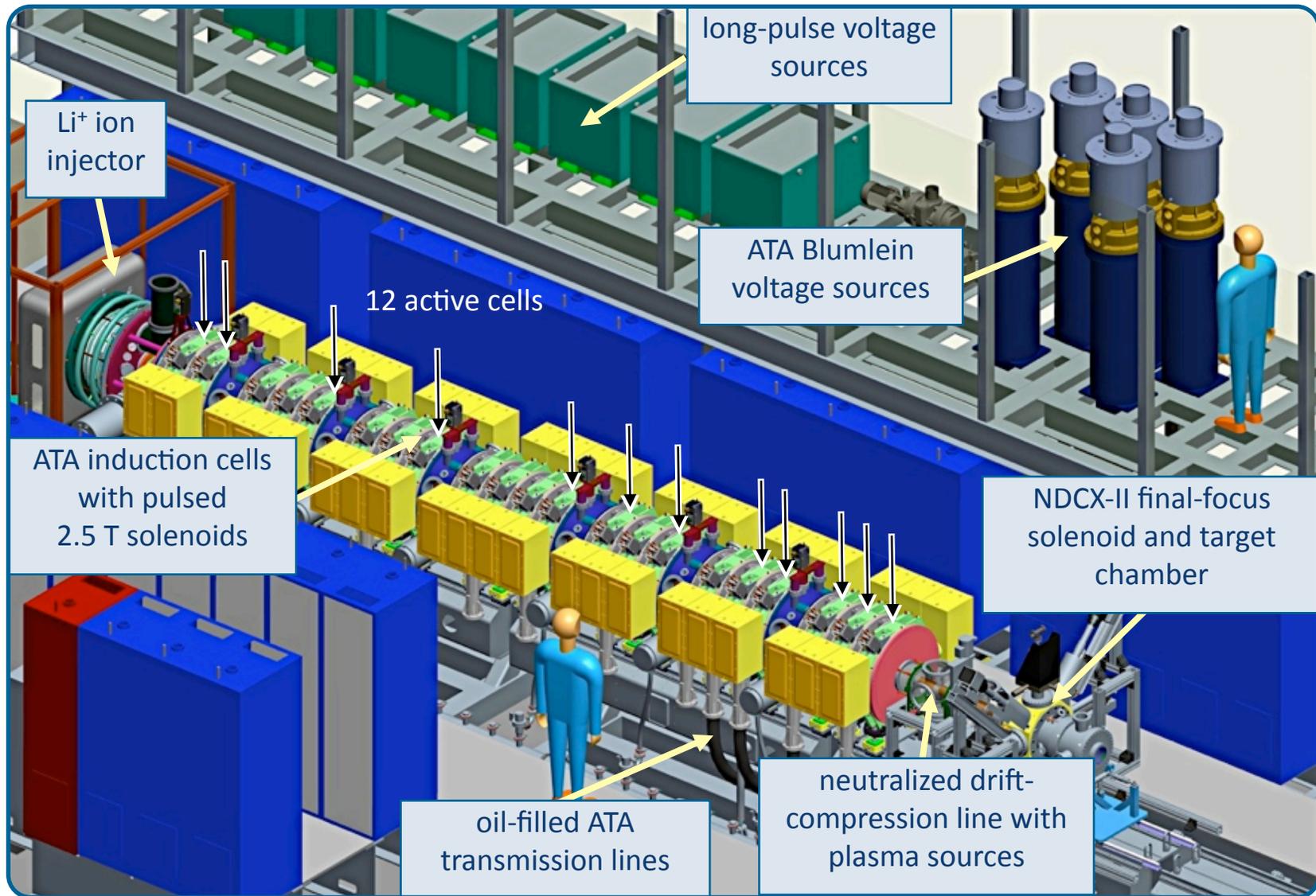


- 27 lattice periods after the injector
- 12 active induction cells
- Beam charge ~50 nano-Coulombs
- FWHM < 1 ns
- Kinetic energy ~ 1.2 MeV

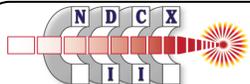
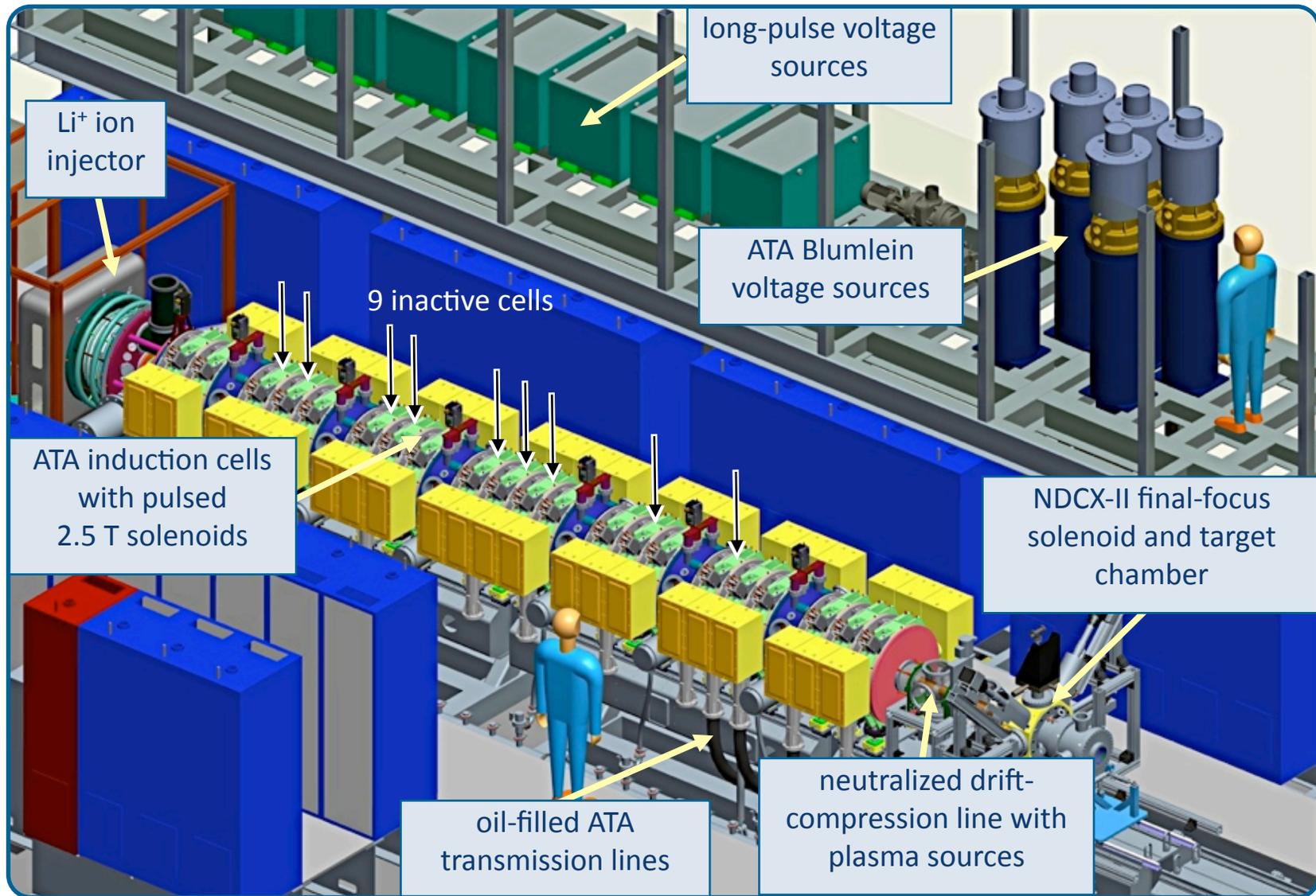
12-cell NDCX-II baseline layout



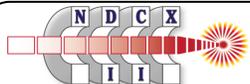
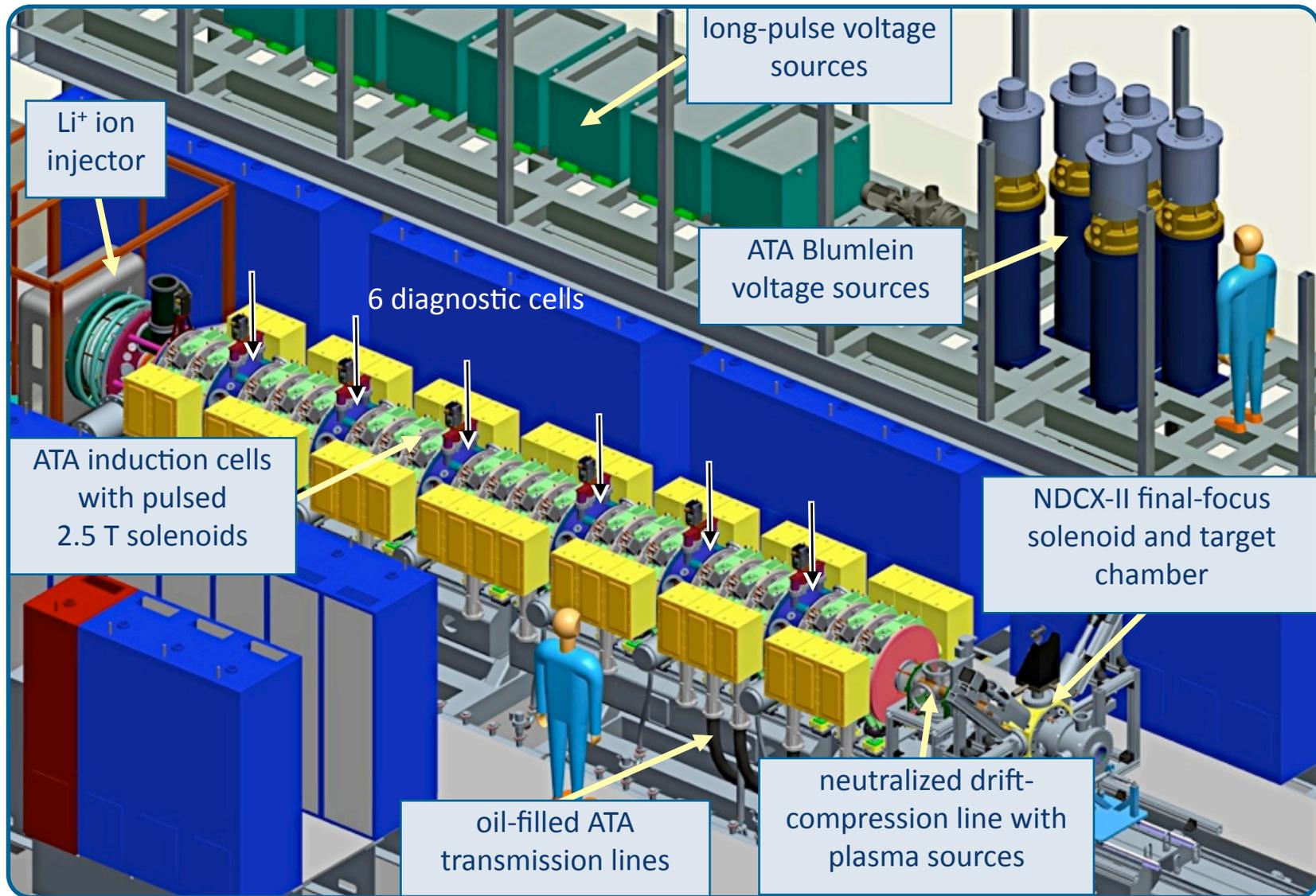
12-cell NDCX-II baseline layout



12-cell NDCX-II baseline layout

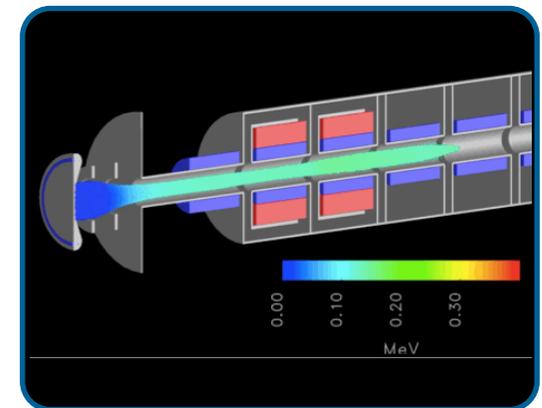
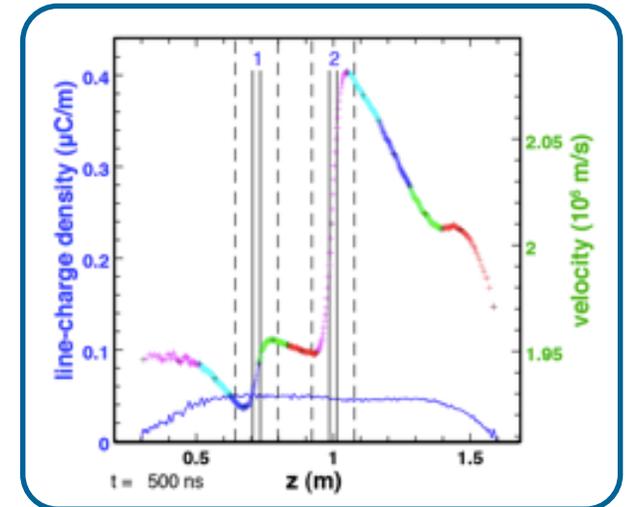


12-cell NDCX-II baseline layout

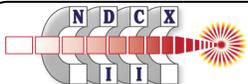


Simulations enabled development of the NDCX-II physics design

- ASP is a purpose-built, fast 1-D (z) particle-in-cell code to develop acceleration schedules
 - 1-D Poisson solver, with radial-geometry correction
 - realistic variation of acceleration-gap fields with z
 - several optimization options
- Warp is our full-physics beam simulation code
 - 1, 2, and 3-D ES and EM field solvers
 - first-principles & approximate models of lattice elements
 - space-charge-limited and current-limited injection
 - cut-cell boundaries for internal conductors in ES solver
 - Adaptive Mesh Refinement (AMR)
 - large Δt algorithms (implicit electrostatic, large $\omega_c \Delta t$)
 - emission, ionization, secondaries, Coulomb collisions...
 - parallel processing

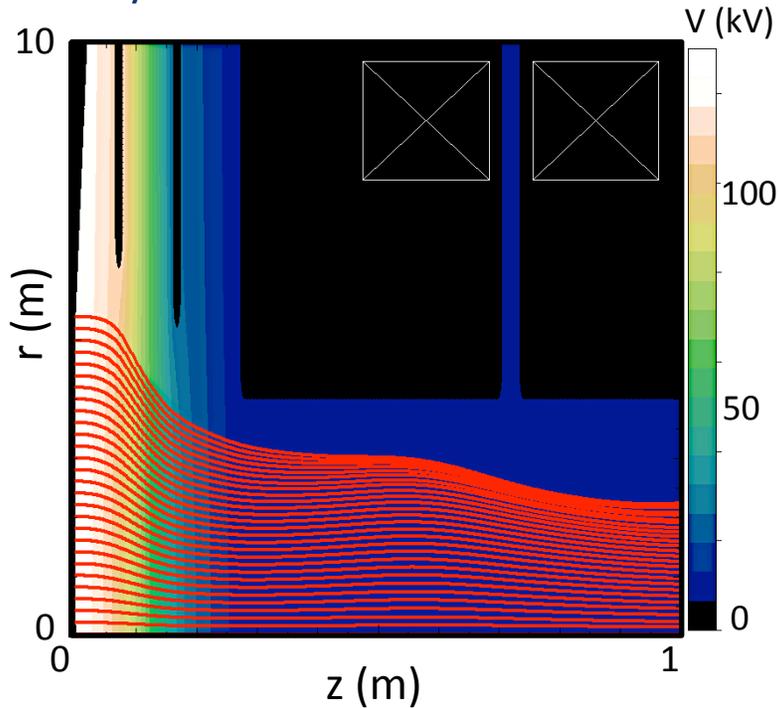


A. Friedman, *et al.*, *Phys. Plasmas* **17**, 056704 (2010).



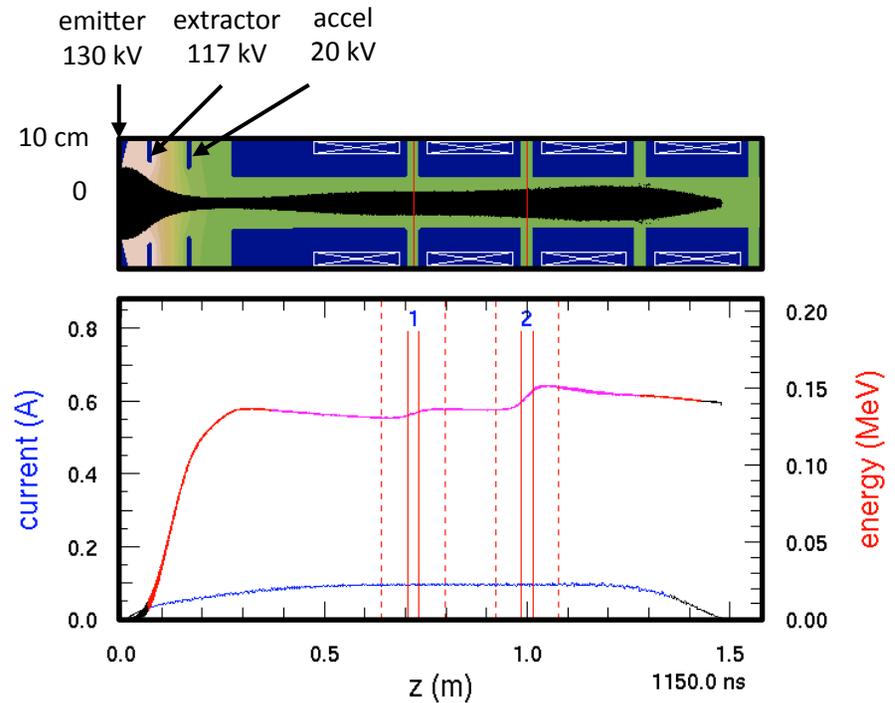
Steps in development of the NDCX-II physics design ...

first, use Warp steady-flow “gun” mode to design the injector for a nearly laminar flow

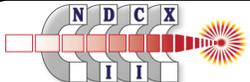


1 mA/cm² Li⁺ ion source

second, carry out a time-dependent *r-z* simulation from the source with Warp

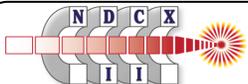
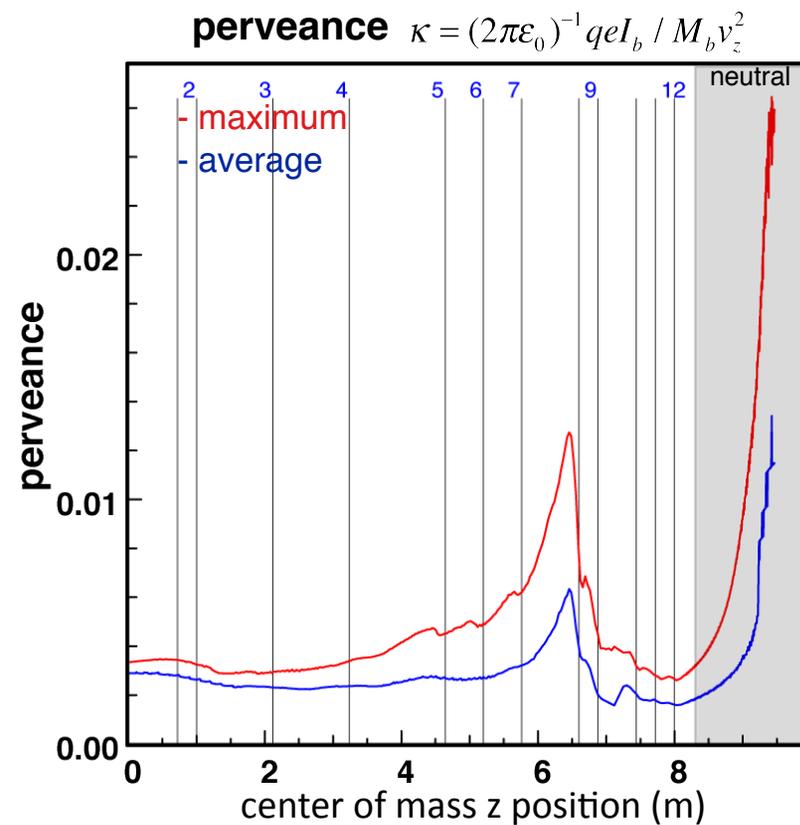
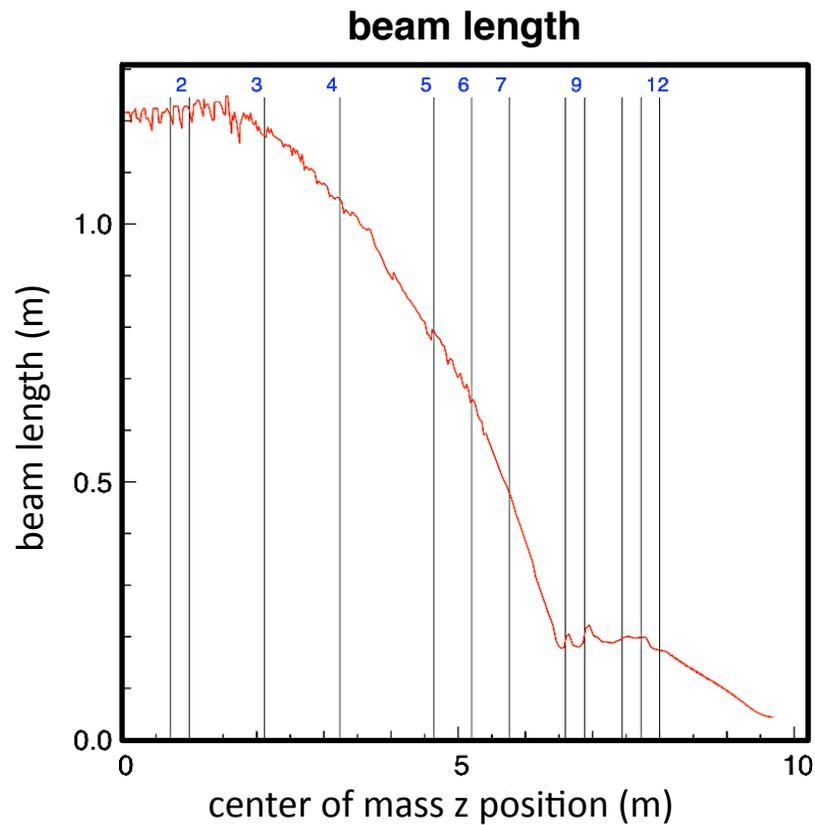


40g-12



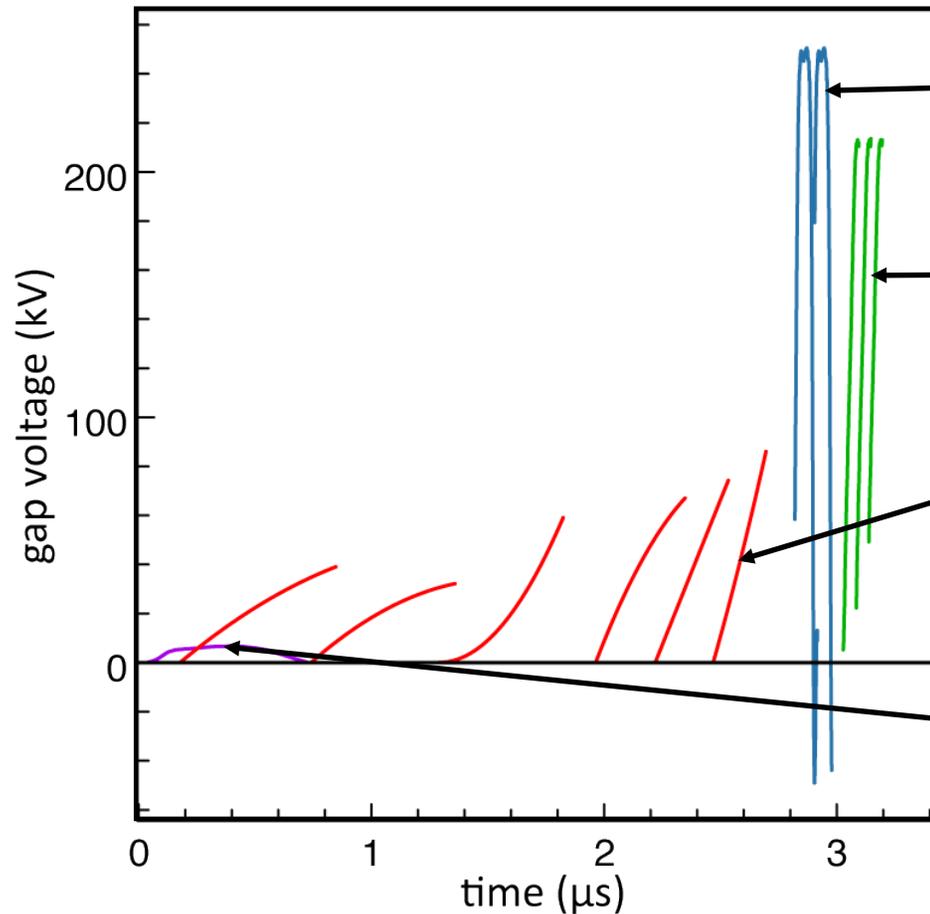
Steps in development of the NDCX-II physics design ...

third, iterate with ASP to find an acceleration schedule that delivers a beam with an acceptable final phase-space distribution



Steps in development of the NDCX-II physics design ...

fourth, pass the waveforms back to Warp and verify with time-dependent r - z simulation



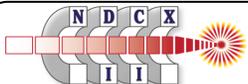
250 kV “flat-top”
measured waveform
from test stand

200 kV “ramp”
measured waveform
from test stand

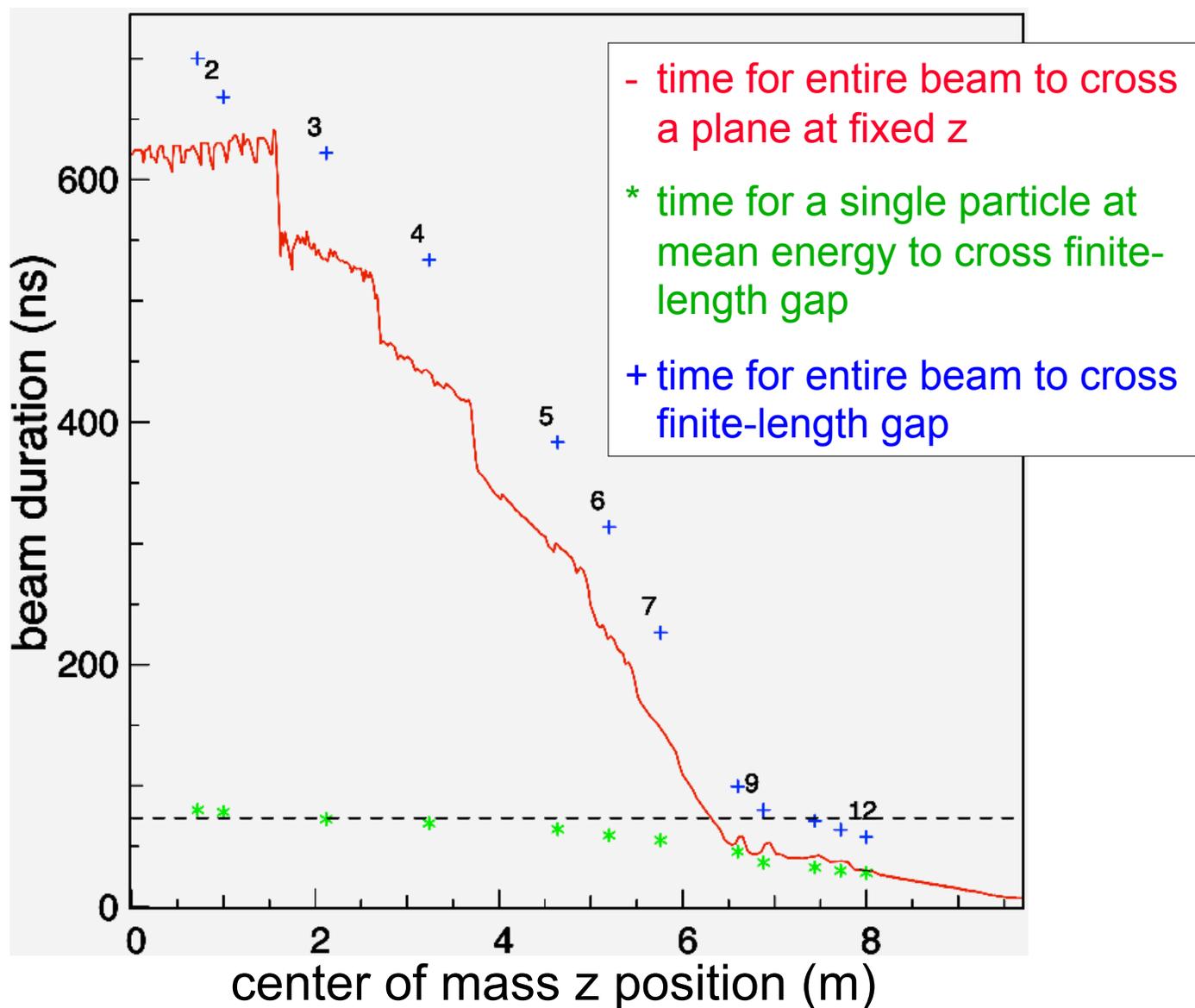
“shaped” for initial
bunch compression
(scaled from measured
waveforms)

“shaped” to equalize
beam energy after
injection

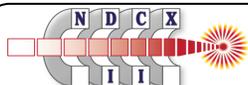
40g.002-12



Pulse duration vs. z: the finite length of the gap field folds in

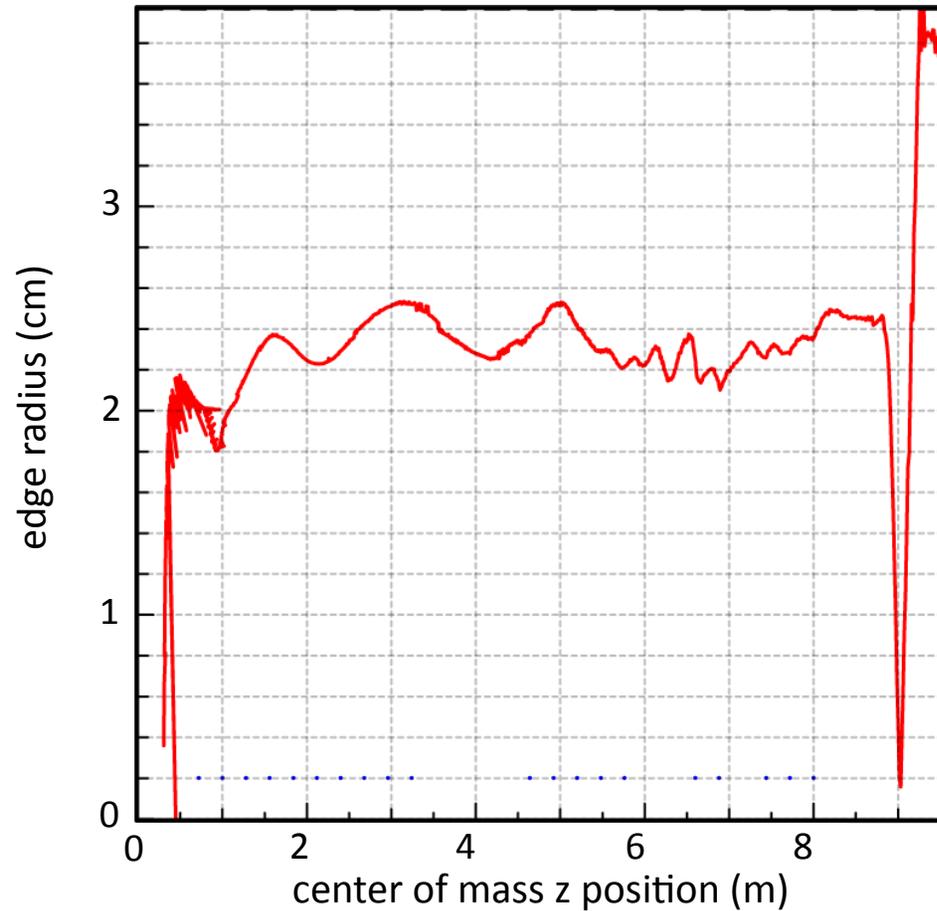


40g.002-12

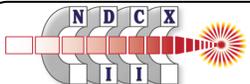


Steps in development of the NDCX-II physics design ...

fifth, adjust transverse focusing to maintain nearly constant radius

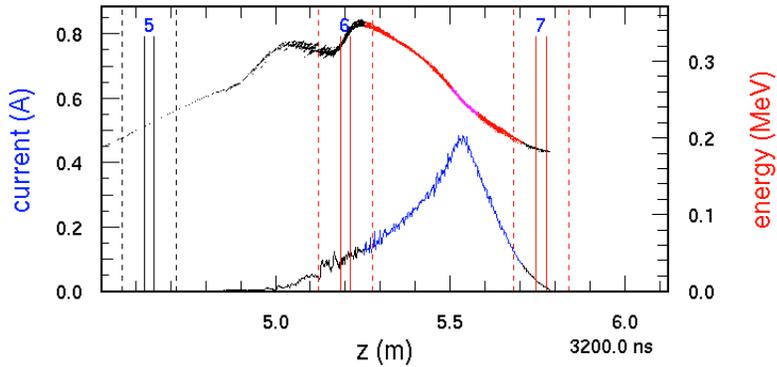
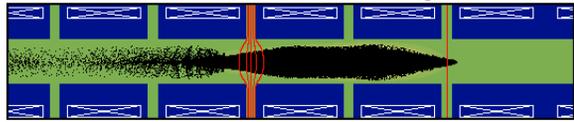


40g.002-12

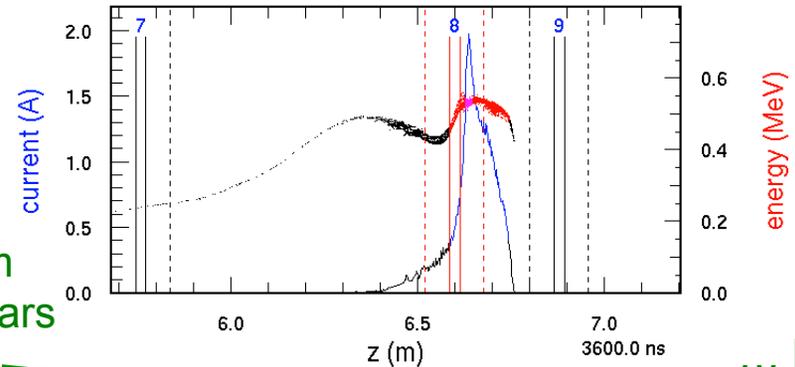
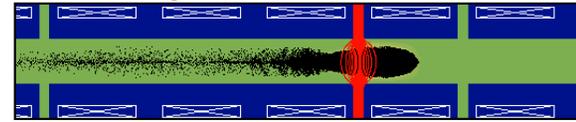


Snapshots from a Warp (r,z) simulation

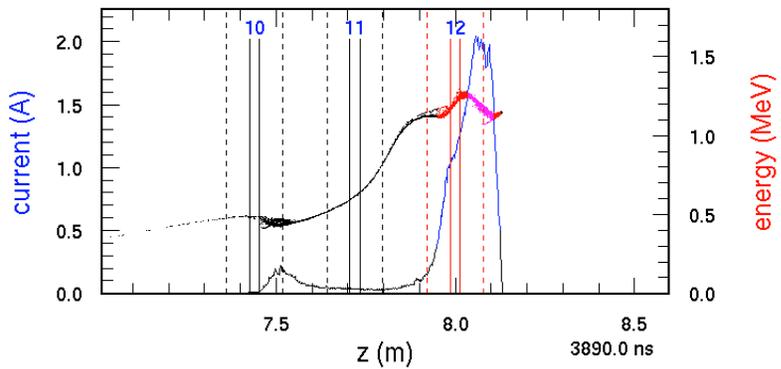
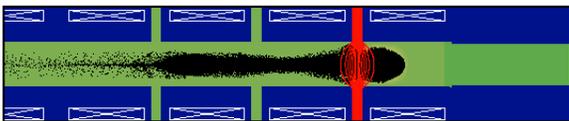
compressing



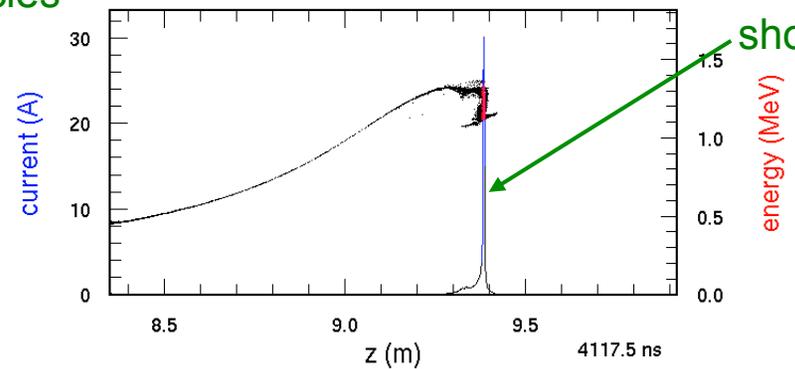
approaching maximum compression



exiting



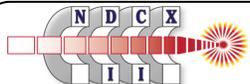
at focus



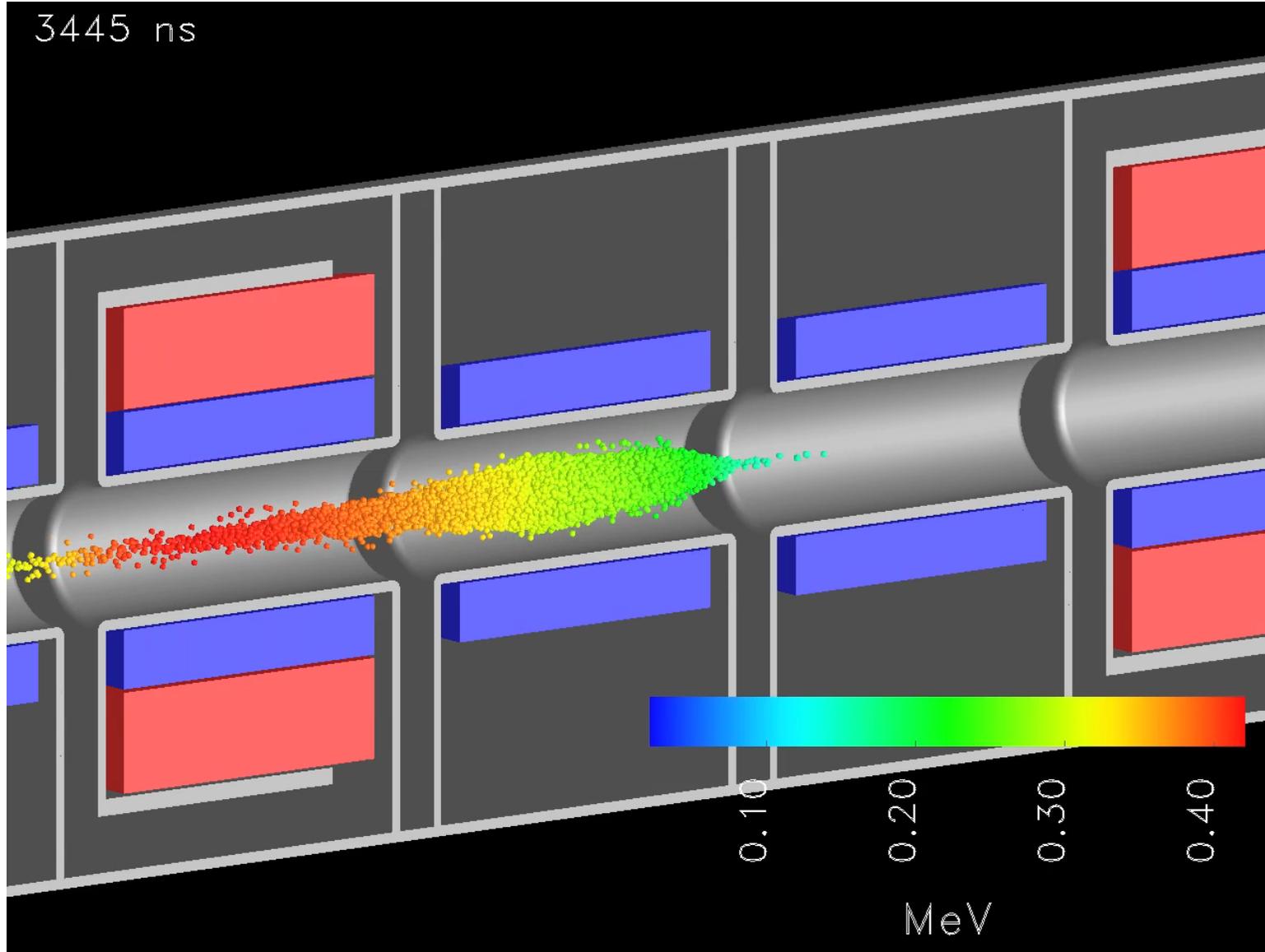
Beam appears long because we plot many particles

...

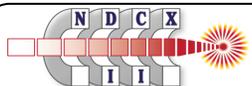
... but current profile shows that it is short



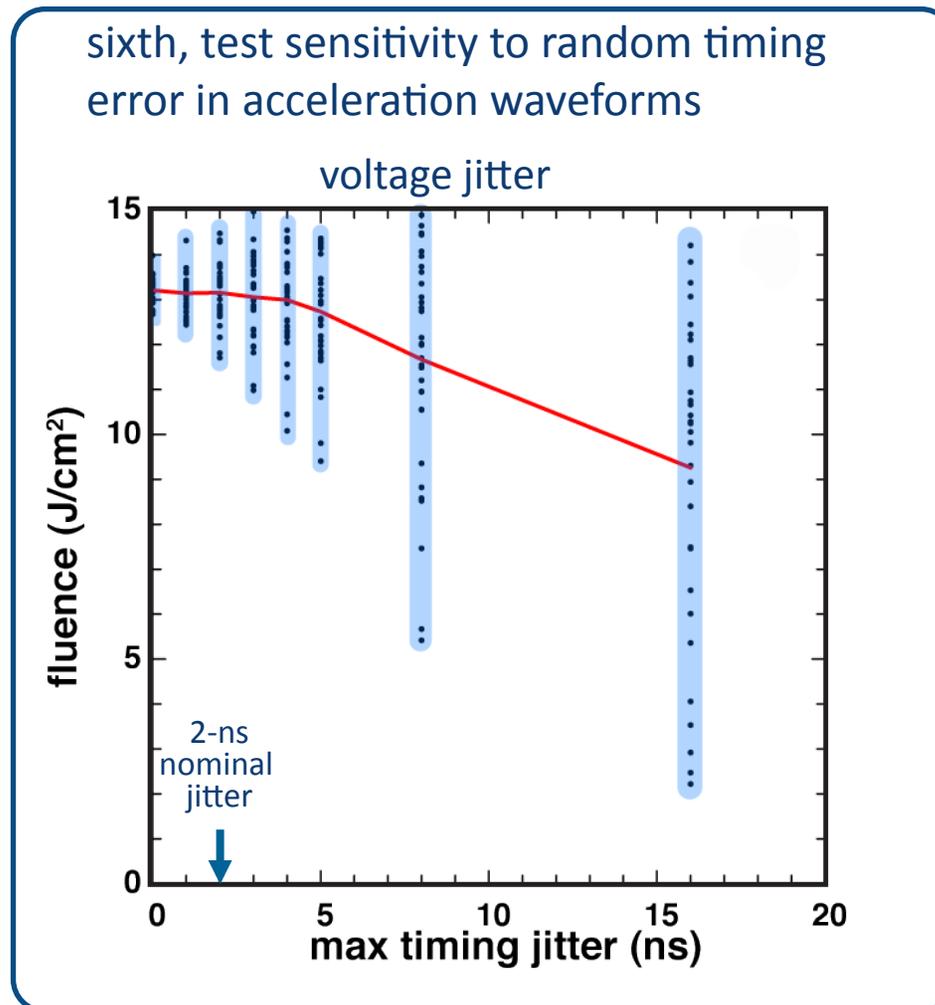
3-D Warp simulation with perfectly aligned solenoids



40ga24-12 simulation and movie from D P Grote

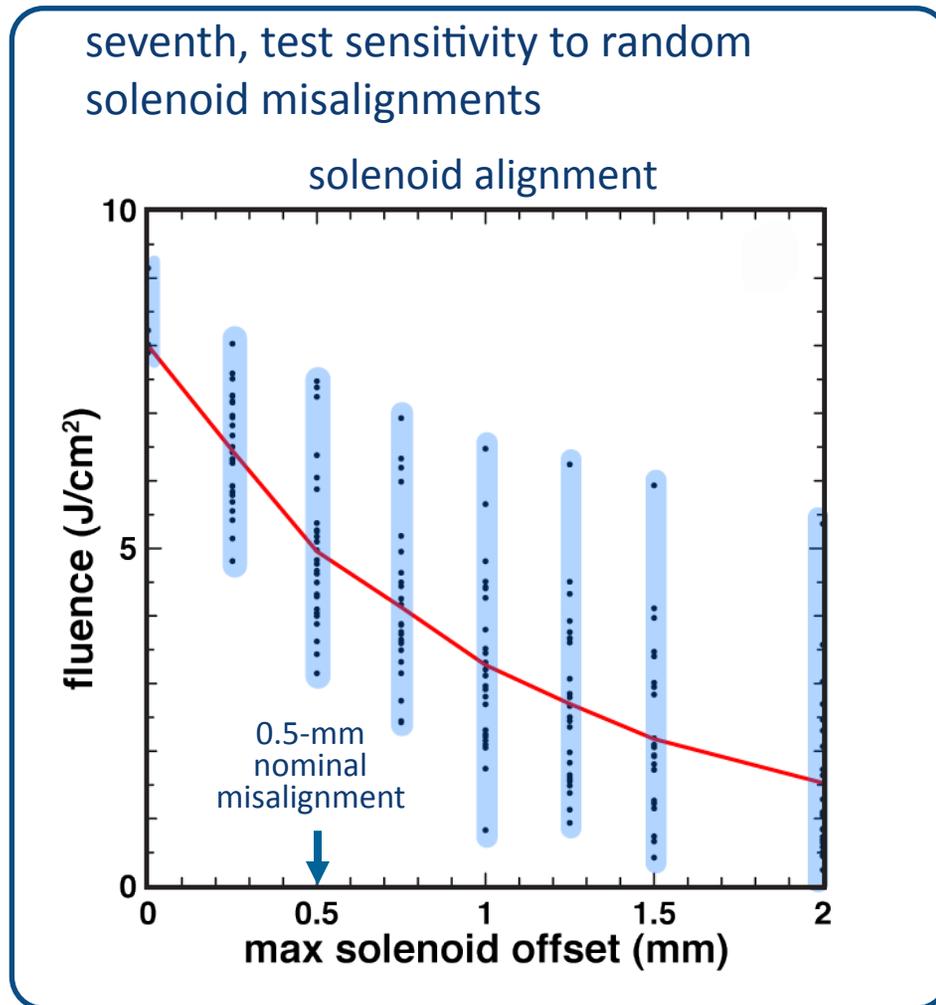


Steps in development of the NDCX-II physics design ...



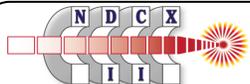
40g-12 with random timing shifts in acceleration voltage pulses

Steps in development of the NDCX-II physics design ...



40g-12 with random offsets to both ends of each solenoid

Beam “steering” via dipole magnets will center beam and minimize “corkscrew” distortion.



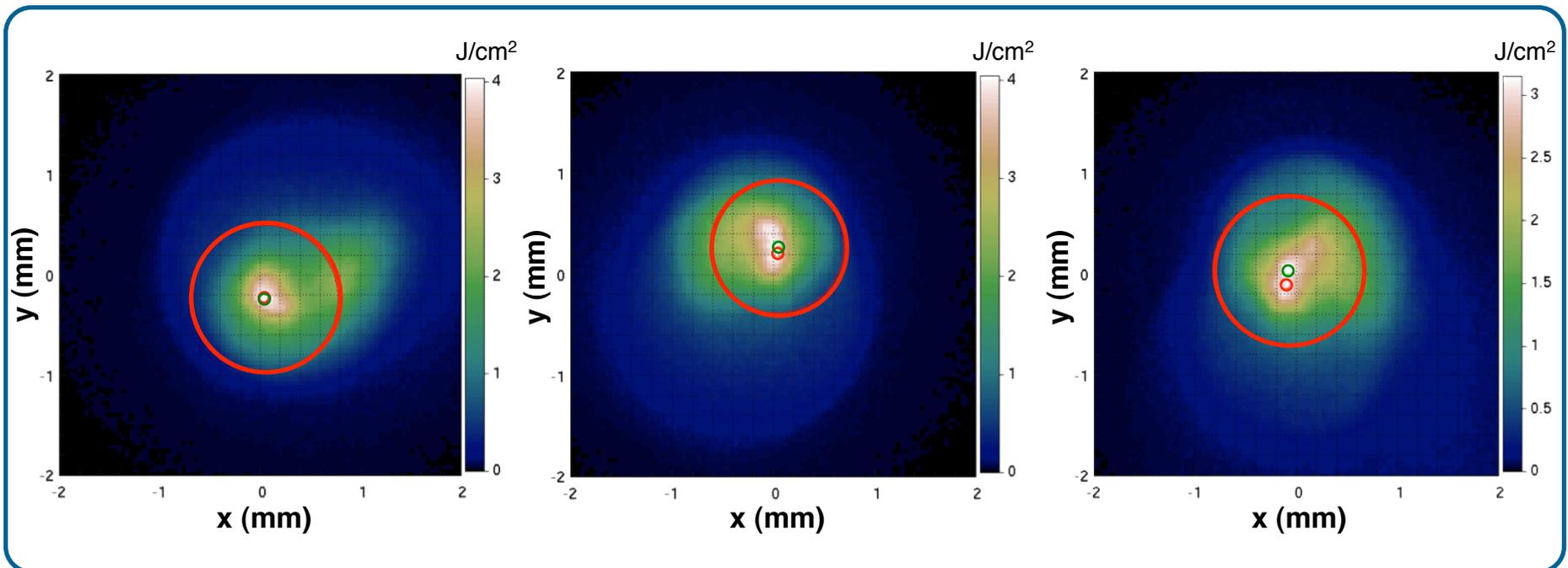
Warp runs illustrate effects of solenoid alignment errors

plots show beam deposition for three ensembles of solenoid offsets

maximum offset for each case is 0.5 mm

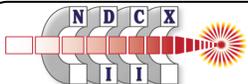
red circles include half of deposited energy

smaller circles indicate hot spots



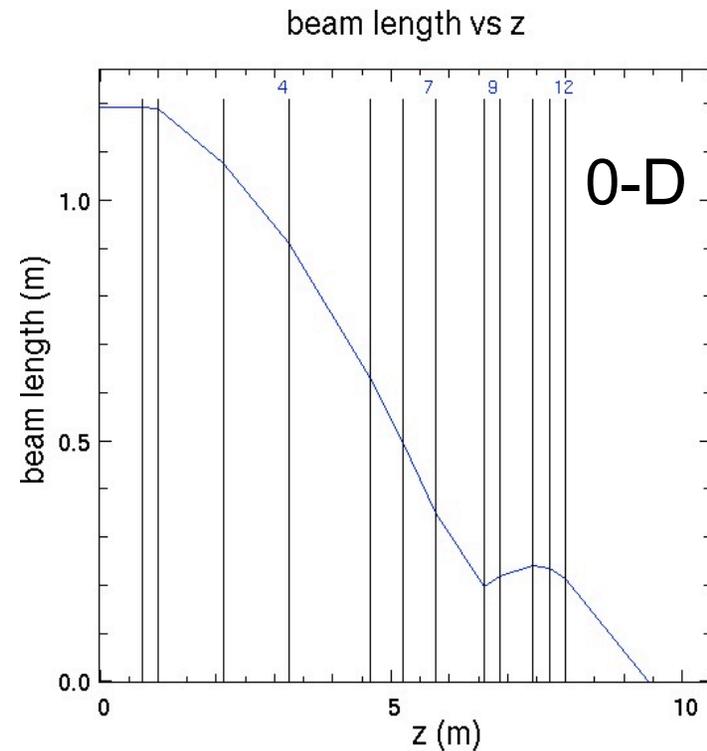
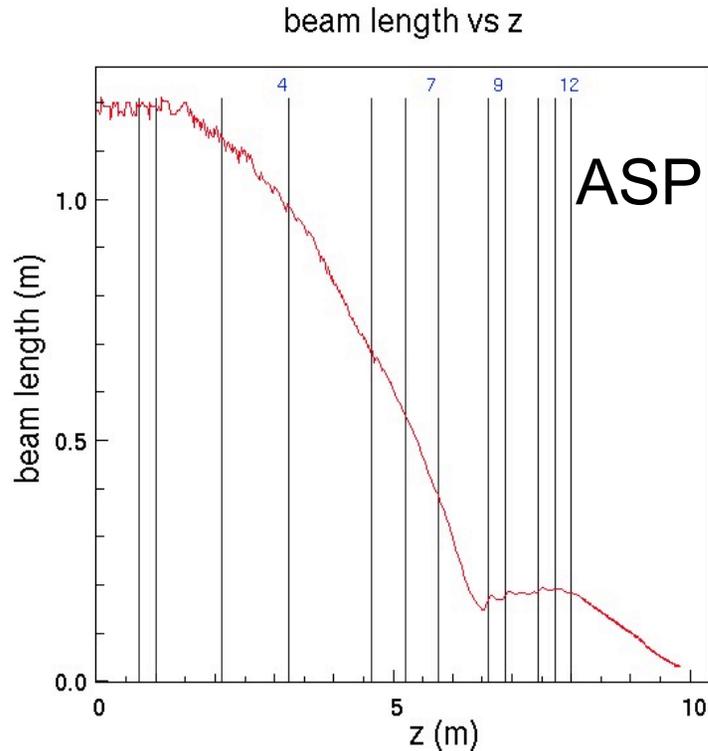
ASP and Warp runs show that steering can improve intensity and stabilize spot location

see Y-J Chen, et al., Nucl. Inst. Meth. in Phys. Res. A 292, 455 (1990)



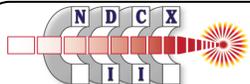
A “zero-dimensional” Python code (essentially, a spreadsheet) captures the essence of the NDCX-II acceleration schedule

- Computes energy jumps of nominal head and tail particles at gaps
- Space-charge-induced energy increments between gaps via a “g-factor” model



- The final head and tail energies (keV) are off; the g-factor model does not accurately push the head and tail outward:
- But – not bad, for a main loop of 16 lines.

	0-D	ASP
head	923	1100
tail	1082	1300



Things we need to measure, and the diagnostics we'll use

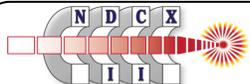
Non-intercepting (in multiple locations):

- Accelerating voltages: voltage dividers on cells
- Beam transverse position: four-quadrant electrostatic capacitive probes
- Beam line charge density: capacitive probes
- Beam mean kinetic energy: time-of-flight to capacitive probes

Intercepting (in two special “inter-cell” sections):

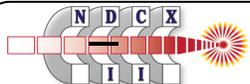
- Beam current: Faraday cup
- Beam emittance: two-slit or slit-scintillator scanner
- Beam profile: scintillator-based optical imaging
- Beam kinetic energy profile: time-of-flight to Faraday cup
- Beam energy distribution: electrostatic energy analyzer

(Underlined items will be available at commissioning)



“Physics risks” concern beam intensity on target, not project completion or risk to the machine due to beam impact

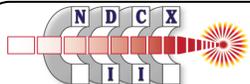
- Alignment errors exceeding nominal 0.5 mm
 - Machine usable with larger errors with intensity degradation
 - Beam “steering,” using dipoles in diagnostic cells, can mitigate “corkscrew” deformation of beam
 - Off-center beam, if reproducible, is not a significant issue
- Jitter of spark-gap firing times exceeding nominal 2 ns
 - Slow degradation of performance with jitter expected, per simulations
 - Similar slow degradation as waveform fidelity decreases
- Source emission non-uniform, or with density less than nominal 1 mA/cm²
 - Simulations show a usable beam at 0.5 mA/cm²
 - Will run in this mode initially, to maximize source lifetime
 - Space-charge-limited emission mode offers best uniformity
- Imperfect neutralization because final-focus solenoid not filled with plasma
 - Build and use a larger-radius solenoid at modest cost to program



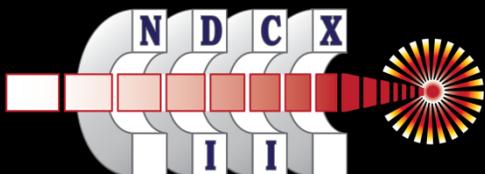
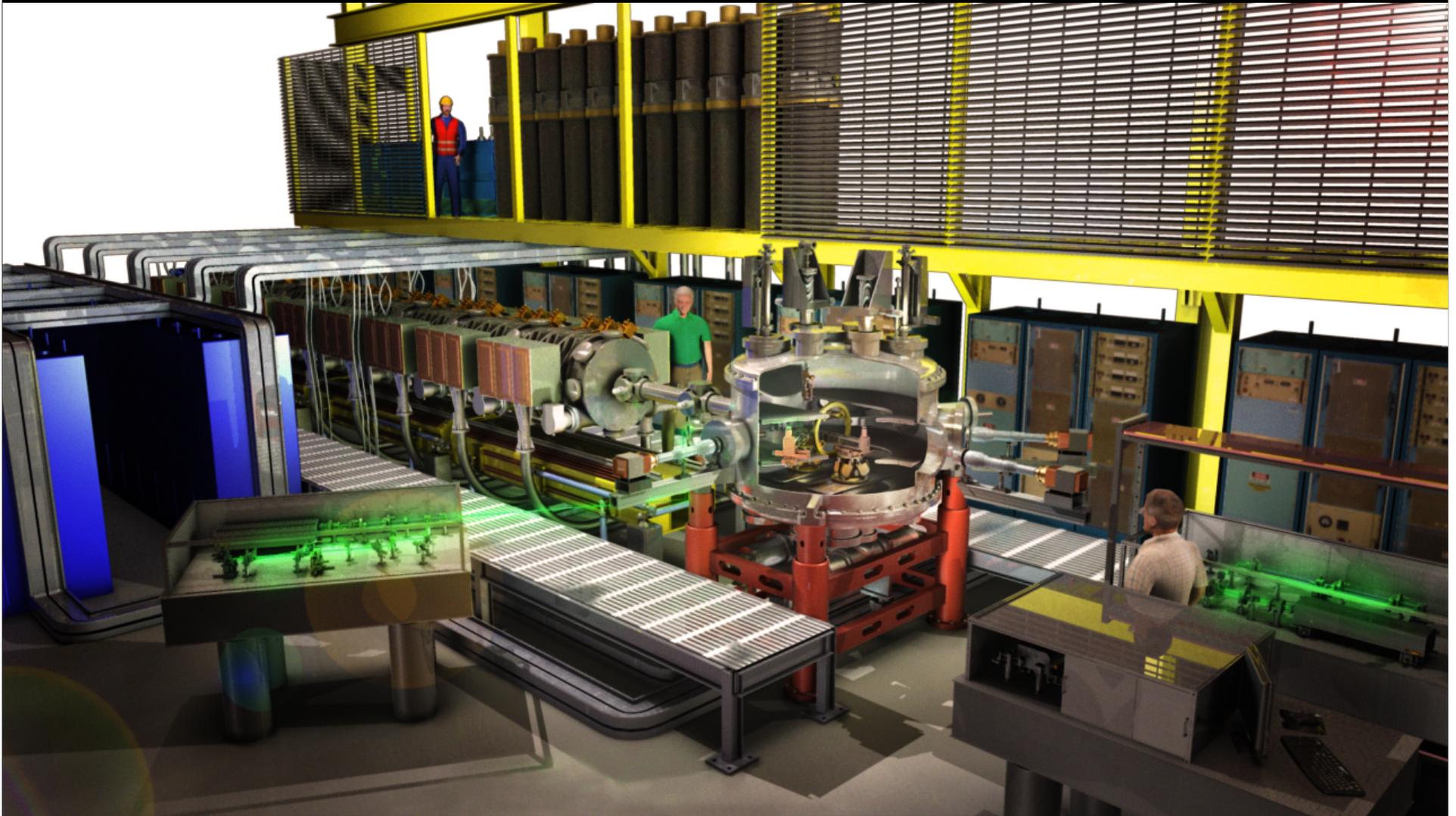
NDCX-II, when mature, should be far more capable than NDCX-I

	NDCX-I (typical bunched beam)	NDCX-II 12-cell (ideal*)
Ion species	K ⁺ (A=39)	Li ⁺ (A=7)
Total charge	15 nC	50 nC
Ion kinetic energy	0.3 MeV	1.25 MeV
Focal radius (containing 50% of beam)	2 mm	0.6 mm
Bunch duration (FWHM)	2 ns	0.6 ns
Peak current	3 A	38 A
Peak fluence (time integrated)	0.03 J/cm ²	8.6 J/cm ²
Fluence within a 0.1 mm diameter spot	0.03 J/cm ² (50 ns window)	5.3 J/cm ² (0.57 ns window)
Fluence within 50% focal radius and FWHM duration ($E_{\text{kinetic}} \times I \times t / \text{area}$)	0.014 J/cm ²	1.0 J/cm ²

* NDCX-II estimates of ideal performance are from (r,z) Warp runs (no misalignments), and assume uniform 1 mA/cm² ion emission, no timing or voltage jitter in acceleration pulses, no jitter in solenoid excitation, and perfect beam neutralization; they also assume no fine energy correction (e.g., tuning the final tilt waveforms)

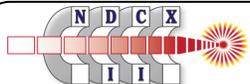


NDCX-II will be a unique user facility for HIF-relevant physics.



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Comments on final beam-lines for a driver



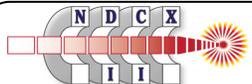
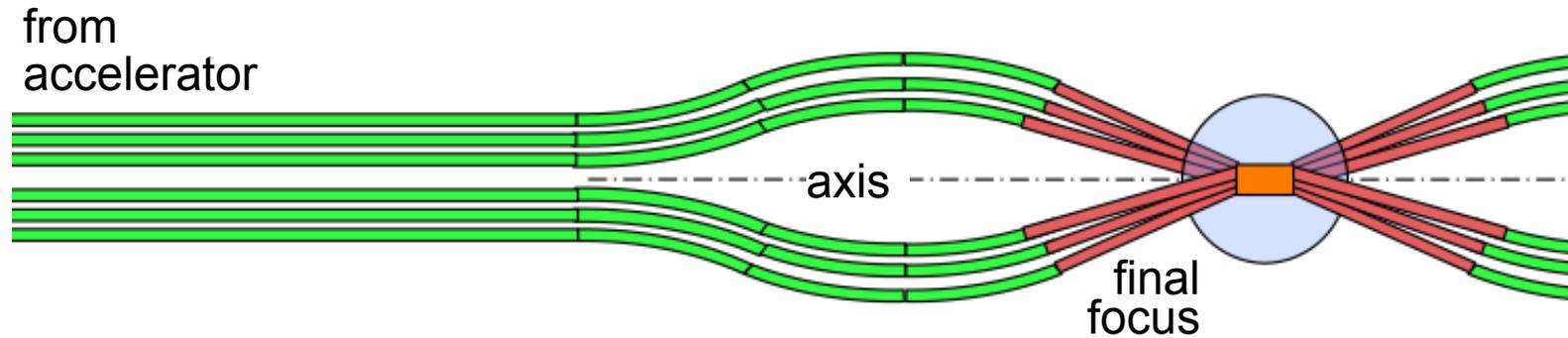
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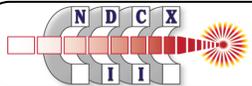
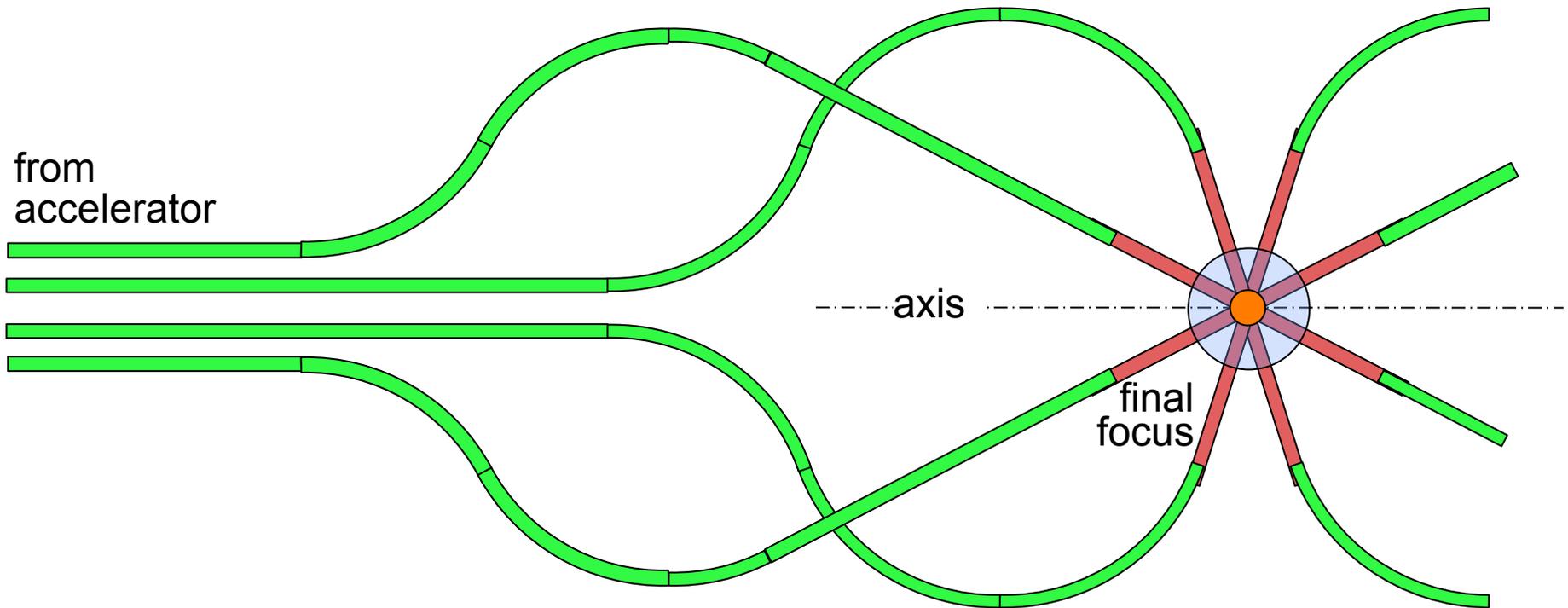
Schematic of final beamlines for ion indirect drive

(only representative
beamlines are shown)



Schematic of final beamlines for ion direct drive

(only representative
beamlines are shown)

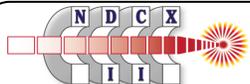
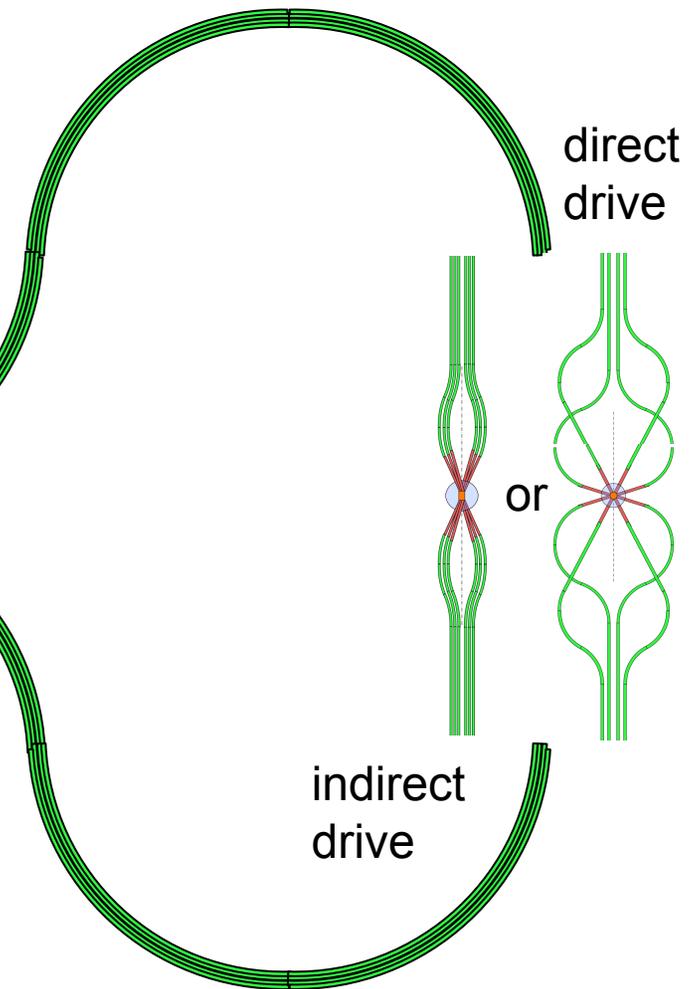


With a single linac, arcs transport the beams to the two sides of the target (for most target concepts)

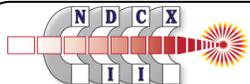
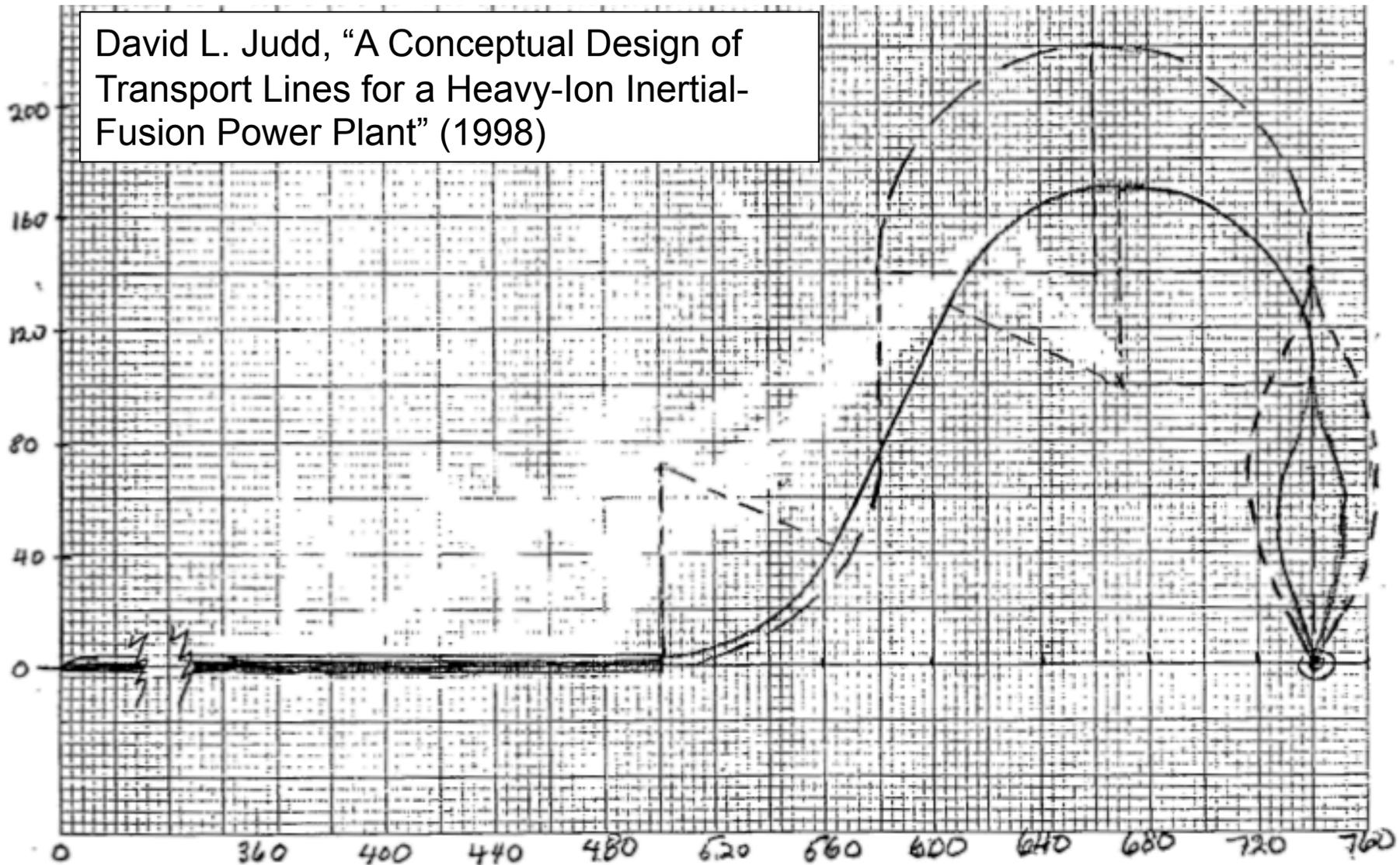
- In the final section of the driver, the beams are separated so that they may converge onto the target in an appropriate pattern.
- They also undergo non-neutral drift-compression, and ultimately “stagnate” to nearly-uniform energy, and pass through the final focusing optic.
- In the scenario examined by Dave Judd (1998), the arcs are ~ 600 m long, while the drift distance should be < 240 m.



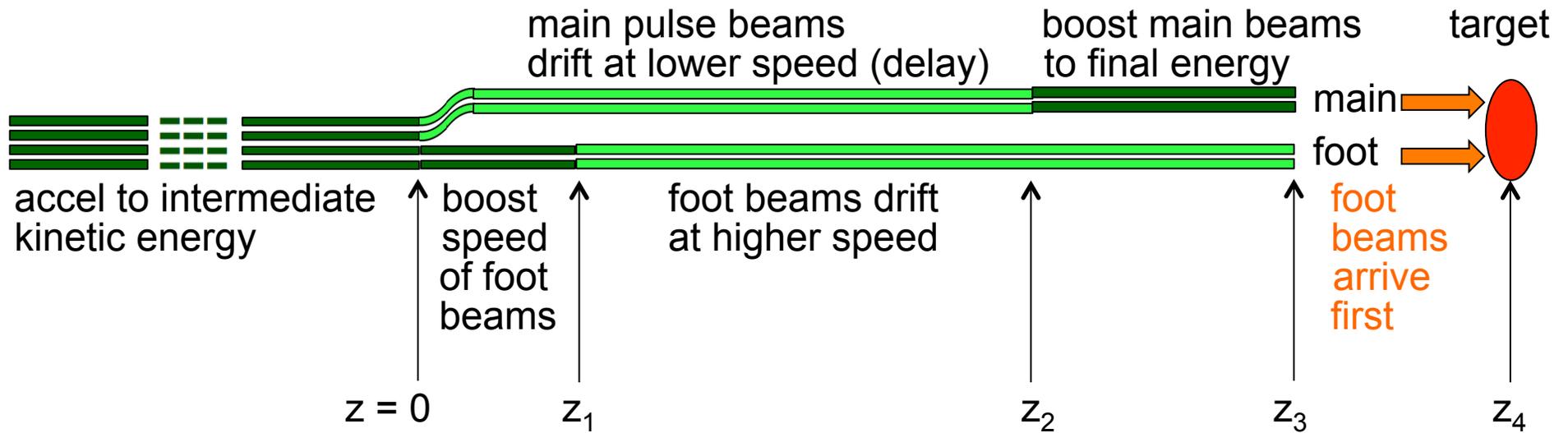
- Thus, the velocity “tilt” must be imposed in the arcs, or upon exit from the arcs.
- To maintain a quiescent beam, “ear fields” are needed in the arcs.
- For pulse-shaping, the arcs may represent an opportunity to pre-configure the beams before final compression.



If a foot pulse of lower K.E. is needed, those beams are “traditionally” extracted from the linac early and routed via shorter arcs

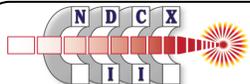


Delay between foot and main pulses can be inserted in a nearly linear system

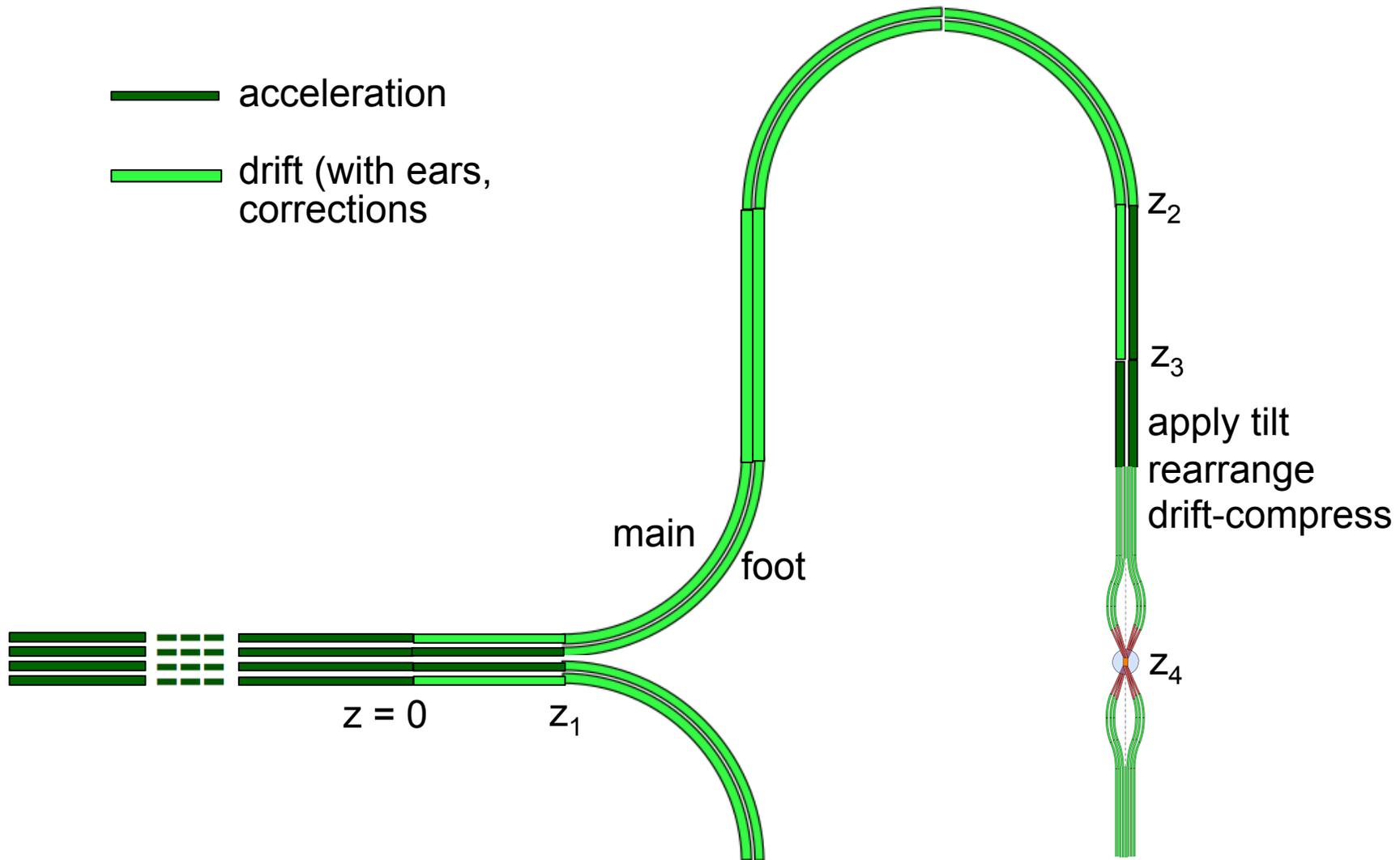


This concept may be useful ...

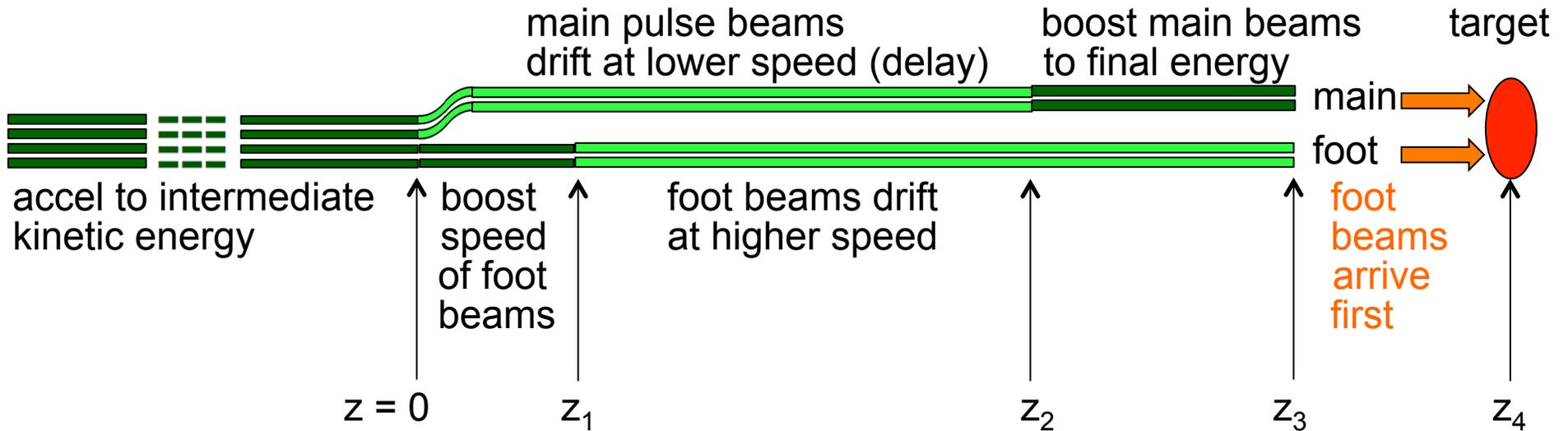
- if two linacs are used, one from each side
- with a single linac, for a single-sided target
- with a single linac, for a two-sided target (see next slide)



A single linac with common arcs could drive a 2-sided target



Example: for an indirect-drive target requiring two beam energies



Aion = 208.980 amu

Accelgradient = 3.0 MV/m

Int. Vz = 48.046 m/us, beta = 0.1603

Foot Vz = 52.632 m/us, beta = 0.1756

Main Vz = 60.774 m/us, beta = 0.2027

Int. Ek = 2.5 GeV

Foot Ek = 3.0 GeV

Main Ek = 4.0 GeV

$z_1 = 0.167$ km

$z_2 = 0.542$ km

$z_3 = 1.042$ km

$z_4 = 1.242$ km

$t_{1\text{foot}} = 3310.884$ ns

$t_{1\text{main}} = 3468.888$ ns

$t_{2\text{foot}} = 10435.840$ ns

$t_{2\text{main}} = 11273.886$ ns

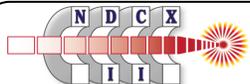
$t_{3\text{foot}} = 19935.780$ ns

$t_{3\text{main}} = 20463.353$ ns

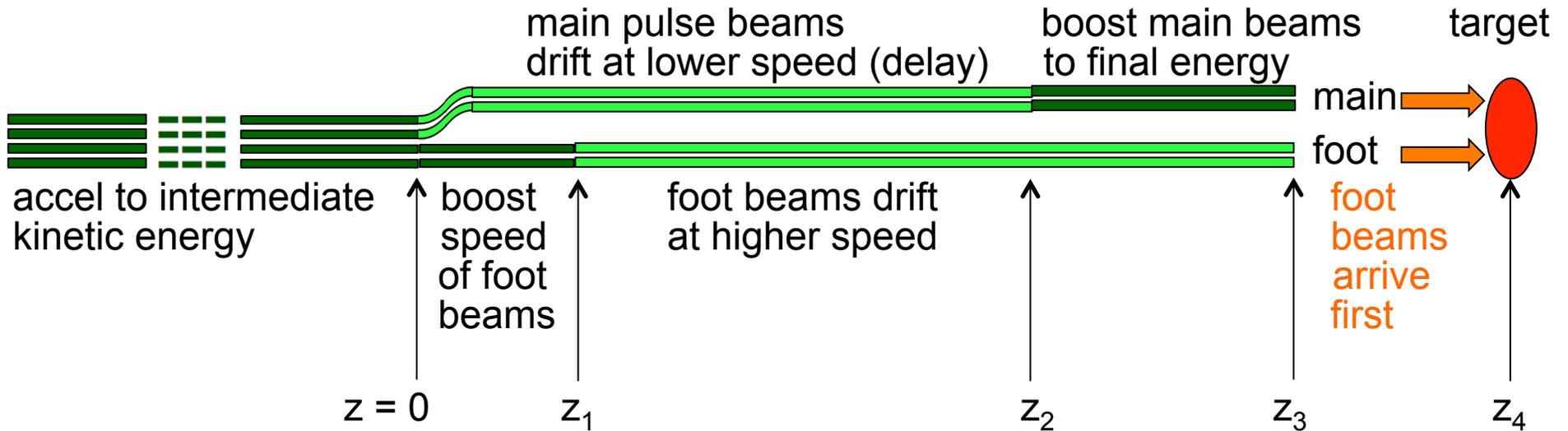
$t_{4\text{foot}} = 23735.757$ ns

$t_{4\text{main}} = 23754.229$ ns

delay = 18.473 ns



Example: for an X-target requiring a single beam energy



Aion = 84.910 amu

Accelgradient = 3.0 MV/m

Int. Vz = 165.140 m/us, beta = 0.5509

Foot Vz = 171.883 m/us, beta = 0.5733

Main Vz = 171.883 m/us, beta = 0.5733

Int. Ek = 12.0 GeV

Foot Ek = 13.0 GeV

Main Ek = 13.0 GeV

z1 = 0.333 km

z2 = 0.433 km

z3 = 0.767 km

z4 = 1.067 km

t1foot = 1978.104 ns

t1main = 2018.490 ns

t2foot = 2559.895 ns

t2main = 2624.038 ns

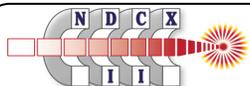
t3foot = 4499.198 ns

t3main = 4602.142 ns

t4foot = 6244.571 ns

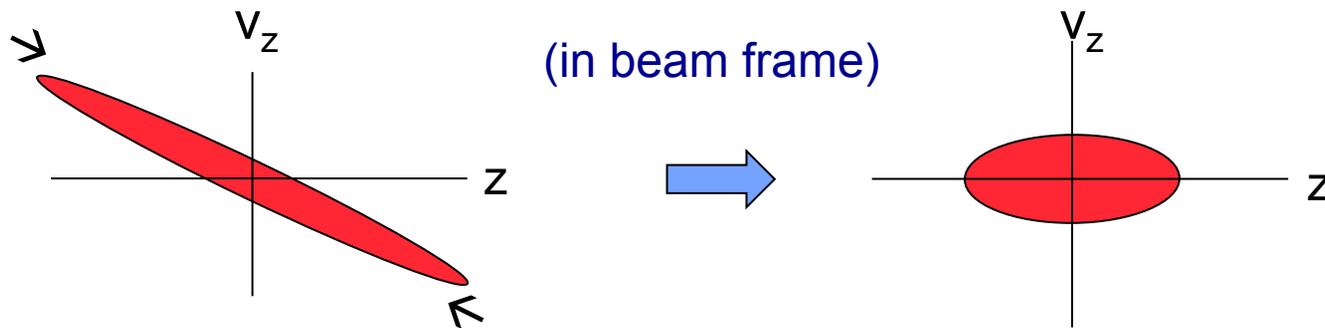
t4main = 6347.515 ns

delay = 102.944 ns

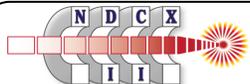
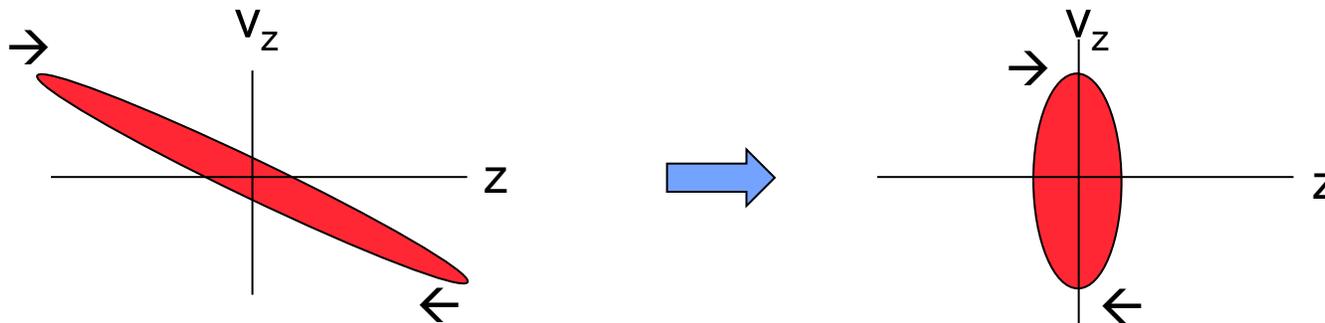


The drift compression process is used to shorten an ion bunch

- Induction cells impart a head-to-tail velocity gradient (“tilt”) to the beam
 - The beam shortens as it “drifts” down the beam line
-
- In **non-neutral drift compression**, the space charge force opposes (“stagnates”) the inward flow, leading to a nearly mono-energetic compressed pulse:

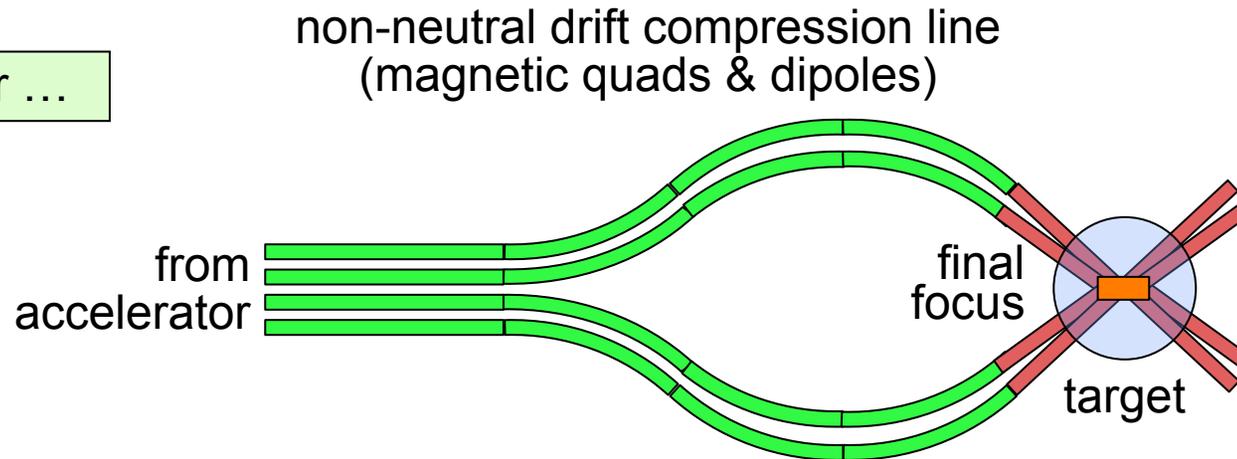


- In **neutralized drift compression**, the space charge force is eliminated, resulting in a shorter pulse but a larger velocity spread:

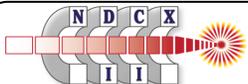
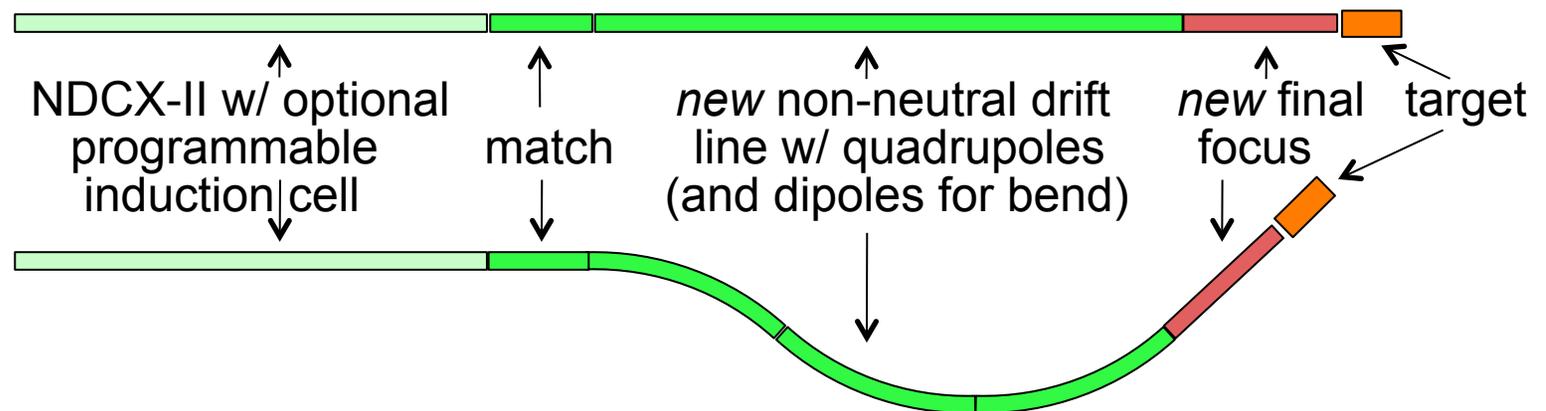


Experiments on NDCX-II can explore non-neutral compression, bending, and focusing of beams in driver-like geometry

In a driver ...



On NDCX-II, two configurations to test ...

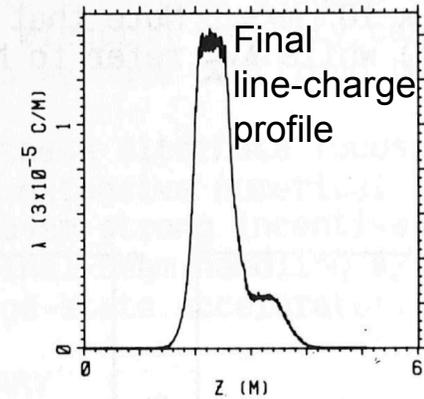
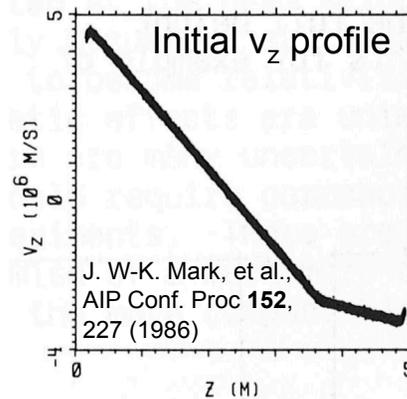


HIF-motivated beam experiments on NDCX-II can study ...

- How well can space charge “stagnate” the compression to produce a “mono-energetic” beam at the final focus?



- How well can we pulse-shape a beam during drift compression (vs. the Robust Point Design’s “building blocks”)?



- How well can we compress a beam while bending it?:
 - “achromatic” design, so that particles with all energies exit bend similarly
 - or, leave some chromatic effect in for radial zooming
 - emittance growth due to dispersion in the bend
- Are there any issues with final focus using a set of quadrupole magnets?

Most dimensionless parameters (perveance, “tune depression,” compression ratio, etc.) will be similar to, or more aggressive than, those in a driver.

