

JPE Problem 1 - Larmor Frame

✓ For a uniform solenoidal channel:

$$B_z^a(s) = B_0 = \text{const}$$

with no acceleration

$$\gamma_b \beta_b = \text{const}$$

and an axisymmetric ( $\partial/\partial\theta = 0$ ) beam with

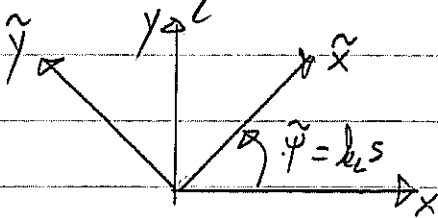
$$\frac{\partial\phi}{\partial\vec{x}_\perp} = \frac{\partial\phi}{\partial r} \frac{\partial r}{\partial\vec{x}_\perp} = \frac{\partial\phi}{\partial r} \frac{\vec{x}_\perp}{r} \quad r = \sqrt{x^2 + y^2}$$

the particle equations of motion reduce to:

$$x'' = \frac{qB_0}{m\gamma_b\beta_b c} y' - \frac{q}{m\gamma_b^3\beta_b^2 c^2} \frac{\partial\phi}{\partial r} \frac{x}{r}$$

$$y'' = -\frac{qB_0}{m\gamma_b\beta_b c} x' - \frac{q}{m\gamma_b^3\beta_b^2 c^2} \frac{\partial\phi}{\partial r} \frac{y}{r}$$

a) Parallel steps taken in the class notes to transform the equations of motion to a co-rotating frame:



$k_L = \text{const} = \text{Larmor Wavenumber}$

$$\begin{aligned} \tilde{x} &= x \cos(k_L s) + y \sin(k_L s) \\ \tilde{y} &= -x \sin(k_L s) + y \cos(k_L s) \end{aligned}$$

Find an expression for  $k_L$  to reduce the equations of motion to the decoupled form:

# TPE Problem 1

Si.M. Lond

P1a/

$$\tilde{x}'' + R\tilde{x} = \frac{-g}{\mu_0 \beta_0 c^2} \frac{\partial \phi}{\partial r} \frac{\tilde{x}}{r}$$

$$\tilde{y}'' + R\tilde{y} = \frac{-g}{\mu_0 \beta_0 c^2} \frac{\partial \phi}{\partial r} \frac{\tilde{y}}{r}$$

and identify  $R = \text{const.}$

Hint:

The transformation can be carried out directly, but you may find the algebra simpler using complex coordinates as in the class notes:

$$\begin{aligned} z &= x + iy \\ \tilde{z} &= \tilde{x} + i\tilde{y} \end{aligned}$$

$$i = \sqrt{-1}$$

$$e^{i\theta} = \cos\theta + i\sin\theta$$

b) If the direction of the magnetic field is reversed:

$$B_0 \rightarrow -B_0$$

how will the dynamics be influenced?

c) Neglect space-charge:

$$\phi = 0$$

and sketch a typical orbit in the rotating Larmor frame. Will this orbit appear more complicated in the Laboratory frame? Why?

Bonus: Sketch the orbit taking advantage of simple choices of initial conditions that can always be made through choice of coordinates.

TPE Problem 2Problem #2  
10 Points

S.M. Lund P2/

2) Derive the  $2 \times 2$  transfer matrices  $M(s|s_i)$  advancing the particle orbit  $x(s)$ ,  $x'(s)$  from the initial conditions at  $s = s_i$

$$x(s_i) \equiv x_i'$$

$$x'(s_i) \equiv x_p'$$

$$\begin{pmatrix} x(s) \\ x'(s) \end{pmatrix} = M(s|s_i) \begin{pmatrix} x_i' \\ x_p' \end{pmatrix}$$

for the following:

a) Free Drift

equation:  $x'' = 0$

b) Continuous focusing:

equation:  $x'' + k_{po}^2 x = 0$

$$k_{po}^2 = \text{const.} > 0.$$

c) Quadrupole focusing:

equation:  $x'' + k_q x = 0$

$$k_q = \text{const} > 0$$

d) Quadrupole defocusing:

equation:  $x'' - k_q x = 0$

$$k_q = \text{const} > 0$$

e) Verify in cases a) - d) that the Wronskian  $W$  satisfies:

$$W = \det M(s|s_i) = 1$$

TPE Problem 3

Problem #3  
15 Points

S.M. Lund P3/

Thin Lens transfer Matrix for a single particle.

3/

Consider  $R_x = \pm \frac{1}{f} \delta(s-s_0)$  and the equation of motion:

$$x'' + \frac{1}{f} \delta(s-s_0) x = 0$$

$f = \text{const}$  (focal-length)

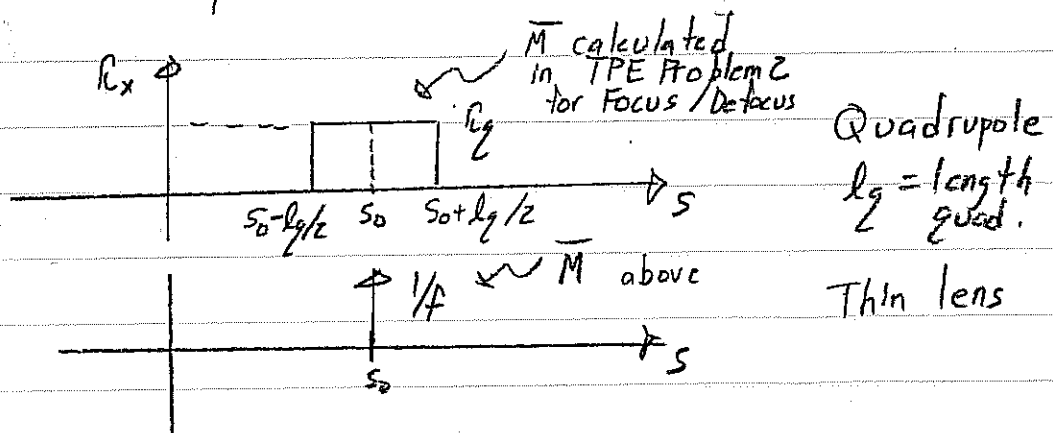
$s_0 = \text{axial location of the optic}$

a) Derive the  $2 \times 2$  transfer matrix  $\bar{M}$  for the optic:

$$\begin{pmatrix} x \\ x' \end{pmatrix}_{s_0^+} = \bar{M} \begin{pmatrix} x \\ x' \end{pmatrix}_{s_0^-}$$

where  $s_0^\pm$  are the coordinates infinitesimally to the left and right of the optic.  $\bar{M}$  is the so-called thin-lens transfer matrix.

b) Construct a thin lens limit for  $2 \times 2$  thick lens transfer matrices for focusing and defocusing quadrupoles with  $R_y = \text{const}$  which obtains the same transfer matrix as in part a).



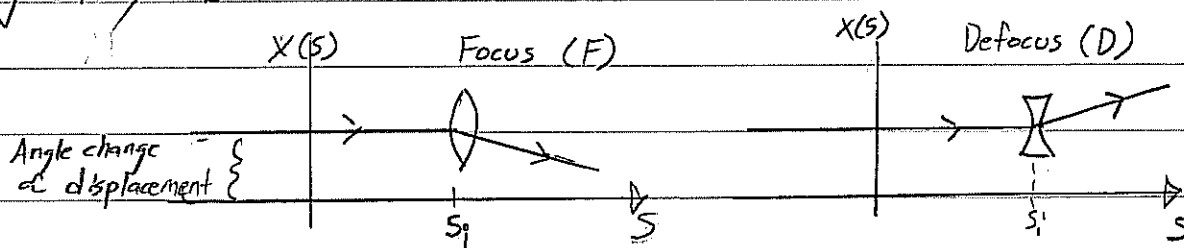
Hint: Require the same "impulse"  $\int ds R_x(s)$  to the particles to relate  $R_y l_g$  and  $f$ , then expand  $\bar{M}$  for focus/defocus quad to get same  $\bar{M}$  as in a).

# TPE Problem 4

Problem #4  
15 Points

S.M. Lund P4/

4/ A thin lense changes the angle of a particle trajectory but not the coordinate:



This action can be specified by transfer matrices applied at  $s=s_1$ :

$$\begin{pmatrix} x \\ x' \end{pmatrix} = M(s_1) \begin{pmatrix} x_1 \\ x_1' \end{pmatrix}$$

Focusing:

$$M_F = \begin{pmatrix} 1 & 0 \\ -\frac{1}{f} & 1 \end{pmatrix}$$

$f > 0$

Defocusing:

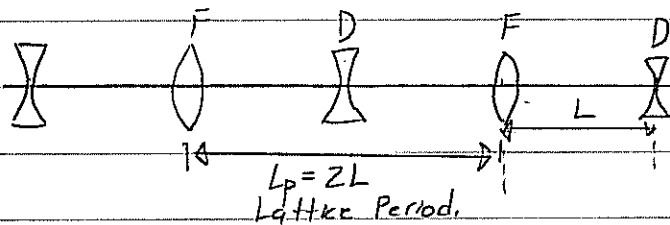
$$M_D = \begin{pmatrix} 1 & 0 \\ \frac{1}{f} & 1 \end{pmatrix}$$

$f > 0$

From TPE Problem 3, free-space drift of length  $L$  has a transport Matrix:

$$M_0 = \begin{pmatrix} 1 & L \\ 0 & 1 \end{pmatrix}$$

Consider a lattice of period  $2L$  made up of equally spaced F and D lenses with equal values of  $f$ .



This is the simplest "FODO" alternating gradient lattice!

- Use the transfer matrix analysis developed in class to find the range of  $f$  for which the particle orbit is stable.
- Calculate  $|\cos \delta_0|$  where  $\delta_0$  is the particle phase advance.

# TPE Problem 4

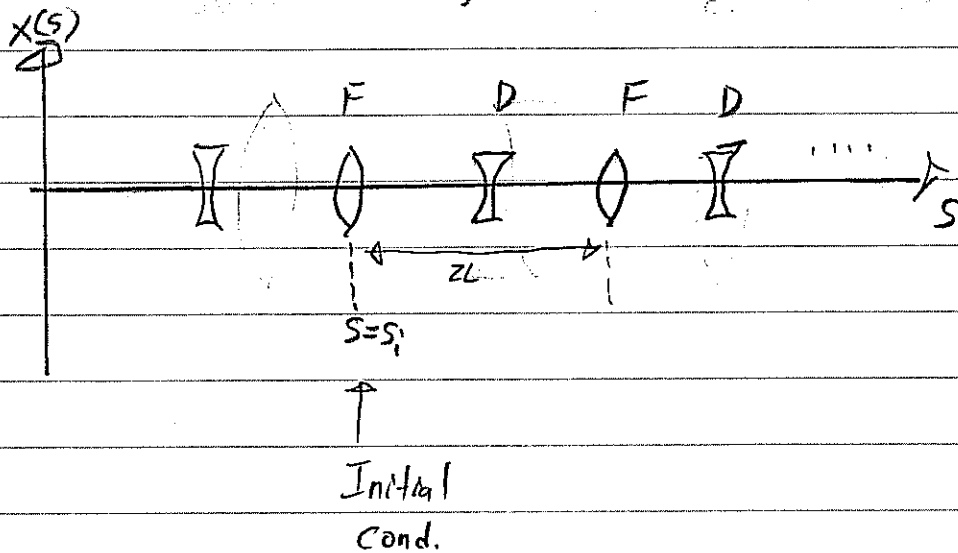
S.M. Lund P4a/

c) For the case of  $f$  chosen to correspond to the stability limit, sketch the motion of a particle with initial condition

$$\lim_{s \rightarrow s_1^-} x(s) = x_0$$

$$\lim_{s \rightarrow s_1^-} x'(s) = \dot{x}_0/L$$

where  $s = s_1$  is the axial location of a focusing thin lens kick, and  $s \rightarrow s_1^-$  is just before the kick. Sketch the particle orbit for  $f$  slightly larger than the stability limit. Superimpose the orbit sketch on a diagram of the lattice (see below):



TPE Problem 5Problem #5  
20 Points

S.M. Lund P5/

5/ Consider a static field magnet with vacuum aperture field satisfying

$$\nabla \cdot \vec{B}^g = 0$$

$$\nabla \times \vec{B}^g = 0$$

Define 2D field components:

$$B_x(x,y) = \frac{1}{l} \int_{-\infty}^{\infty} dz B_x^g(x,y,z)$$

$$B_y(x,y) = \frac{1}{l} \int_{-\infty}^{\infty} dz B_y^g(x,y,z)$$

where  $l = \text{const.}$  is any length scale.

a) Show that the 2D field components satisfy (finite magnet)

$$\frac{\partial B_x(x,y)}{\partial x} = -\frac{\partial B_y(x,y)}{\partial y}$$

$$\frac{\partial B_x(x,y)}{\partial y} = \frac{\partial B_y(x,y)}{\partial x}$$

Cauchy-Riemann conditions for  $B = B_y + i B_x$  to be an analytical function of  $z = x + iy$   $i = \sqrt{-1}$

b) Write out 2D field components for normal and skew component quadrupole and sextupole magnets.

eg. Normal quadrupole  $n=2, b_2 \neq 0, a_2 = 0$

Skew quadrupole  $n=2, b_2 = 0, a_2 \neq 0$ , etc.

c) Using  $\vec{F} = q \beta_0 c \hat{z} \times \vec{B}_\perp$   $\vec{B}_\perp = B_x \hat{x} + B_y \hat{y}$  sketch lines of force acting on a particle with charge  $q$  moving along the  $z$ -axis for a normal quadrupole and then a skew quadrupole. How do these differ?

## TPE Problem 5

S.M. Lund P59/

d) Will the normal and skew terms be defined the same for electric quadrupole focusing or should they be interchanged?

i.e.,

$$\tilde{E} = E_y + i E_x = \sum_{n=1}^{\infty} \tilde{E}_n \left( \frac{z}{r_p} \right)^{n-1}$$

$$\tilde{E}_n \equiv \begin{matrix} a_n + i b_n \\ \text{Skew} \quad \text{Normal} \end{matrix}$$

or

$$\tilde{E}_n \equiv \begin{matrix} b_n + i a_n \\ \text{Normal} \quad \text{Skew} \end{matrix}$$

e) What ideal pole orientation is necessary to generate magnetic normal and skew quadrupole field components? Only sketches are necessary.